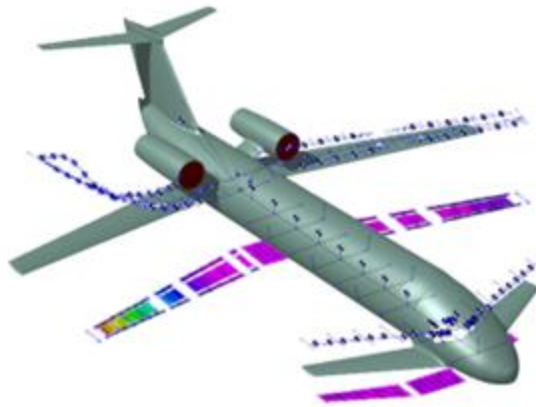


Aeroelastic analysis using NeoCASS and NeoRESP



18 July 2018

NeoCASS 2.2.82

Aeroelastic analysis in NeoCASS/NeoRESP

In NeoCASS are included capabilities for aeroelastic analysis:

- Static aeroelasticity (trim and loads)
- Normal modes
- Flutter analysis

NeoRESP is an additional module used for dynamic response analysis:

- Gust response;
- Control surface deflection response;
- Response to external loads;
- State-space realization of the aeroelastic system.

It features

- Frequency domain solution;
- Time domain solution;
- Mode acceleration for load recovery.



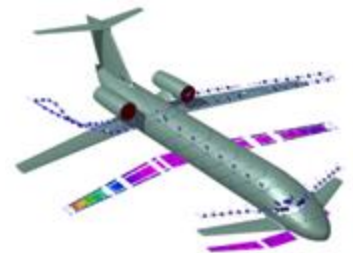
Tutorial overview

This tutorial will introduce some of the capabilities of the code, following the steps:

- Generation of the aircraft model using GUESS
- Linear trim analysis
- Normal mode computation
- Flutter analysis
- Gust response analysis
- Control surface deflection time response
- State-space model generation

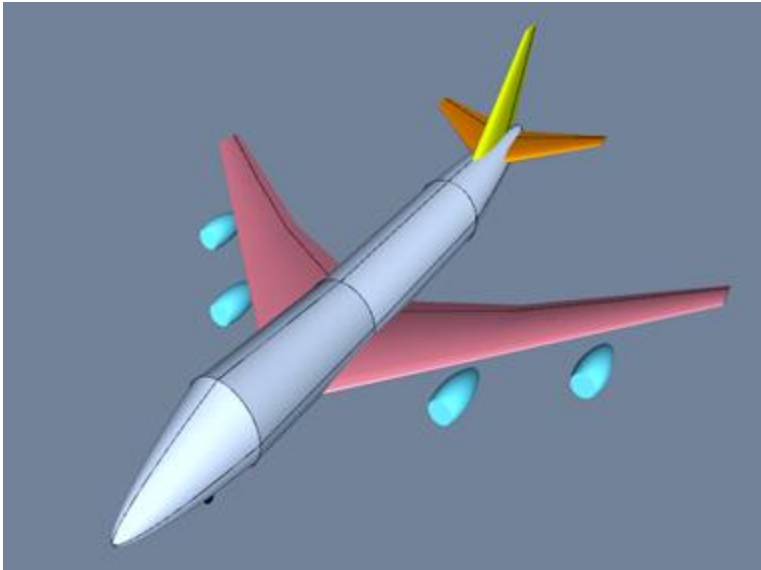
All the procedures will be presented on a model inspired to the B747-100 aircraft. The model data, and the scripts that can be used to reproduce the results presented here can be found in the directory

`<NeoCASS_base>/Examples/B747-100/`



Model generation (1)

The aircraft model in Smartcad format is generated starting from an .xml file with the geometric properties and using GUESS.



The files used in this operation are

- B747-100.xml : geometry input file which can be defined/edited using AcBuilder
- B747-100_CAS25.inc : maneuver definition for structural sizing

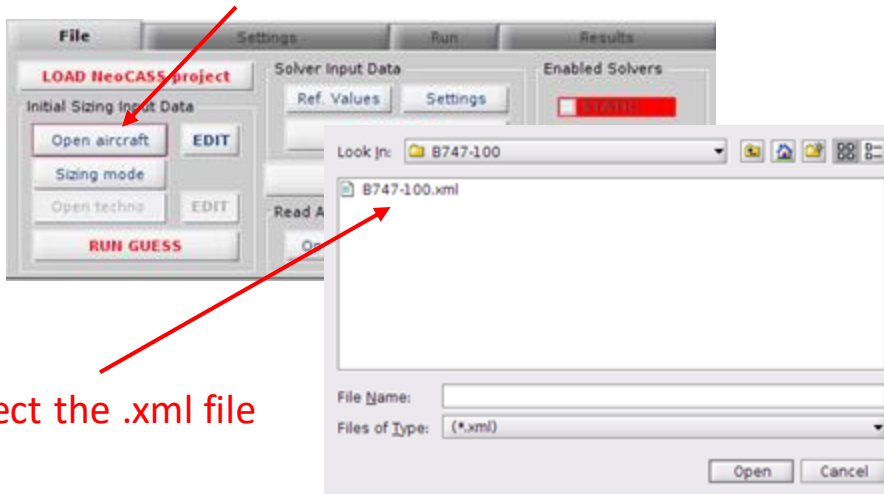
The operation can be performed either using the NeoCASS GUI (NeoCASS command) or programmatically (the commands can be found in the script `exampleMain_guess.m`).



Model generation (2)

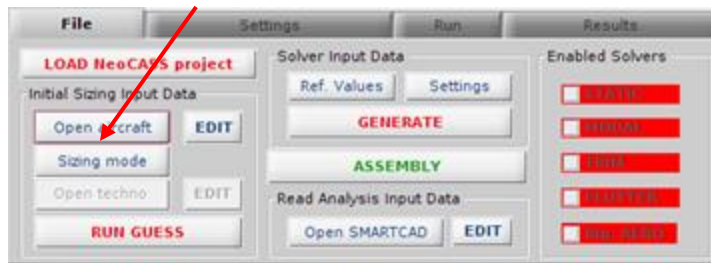
GUI

Select Open aircraft button



Select the .xml file

Select Sizing mode button



Command line

Define the .xml files

```
filename_geo = 'B747-100.xml';  
filename_tech = 'B747-100.xml';
```



Model generation (3)

GUI

Guess/SMARTCAD trim interface

Pullup Horizontal tail/canard Vertical tail
 Ailerons Static Gust Taildown Landing
 Engine Out High Lift

Cruise altitude (HCRU) [m]:
Min cruise mach number (MCRU) []:
Max ceiling altitude (HMAX) [m]:
Clean max lift coefficient (CLMAX) []:
All flaps down max CL at Take Off (CLMAXTO) []:
All flaps down max CL at Landing (CLMAXLAND) []:
Clean lift curve slope (CLALPHAD) []:
Reference surface (USERSREF) [m²]:
Flap deflection for TO (FLAPTO) [deg]:
Flap deflection for Landing (FLAPLAND) [deg]:
Sink speed at landing (VSINK) [m/s]:
Shock absorber stroke at landing (STROKE) [m]:
Landing gear efficiency (LNDGEFF) []:

Maneuvers set definition
Number of flight conditions:

Export to:

Load trim conditions from file

Solution Method
 Rigid Aircraft joined wing
 Elastic Aircraft

Select "Load trim conditions from file" option

Leave default parameters for solution method

Select the file B747-100_CAS25.inc

Command line

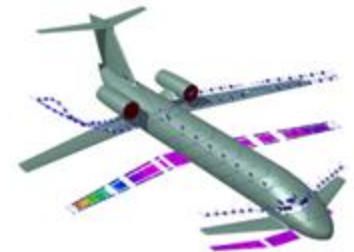
Define the .inc file for maneuver definition

```
filename_trim = 'B747-100_CAS25.inc';
```

Define the solution method

```
model.Joined_wing = false;  
model.Strut_wing = false;  
model.EnvPoints = [];  
model.guessstd = false;
```

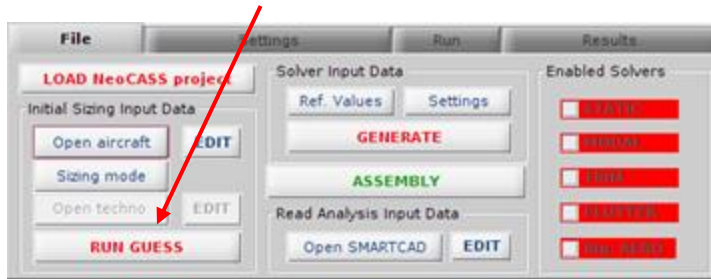
True : Rigid aircraft
False : elastic aircraft



Model generation (4)

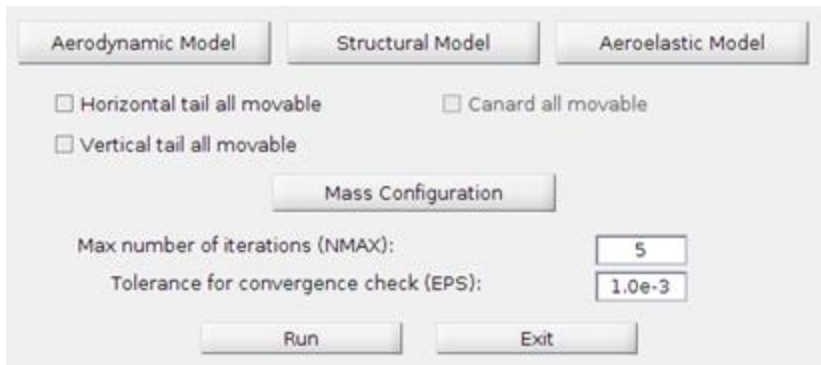
GUI

Select RUN GUESS button



Specify the name of the generated files
(e.g. B747-100_v00.inc)

The ChEcK GUI will appear



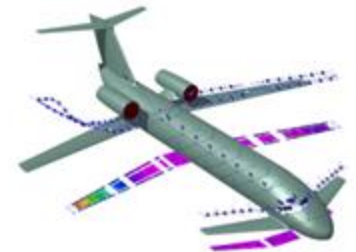
Command line

Determine whether to use or not the ChEcK GUI (true: the ChEcK GUI will appear)

```
sizinginBatch = false;
```

Define the name of the generated model file

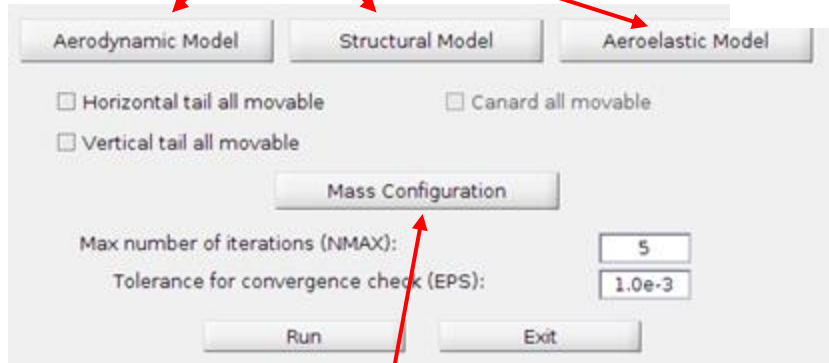
```
filename_stick = 'B747-100_v00.inc';
```



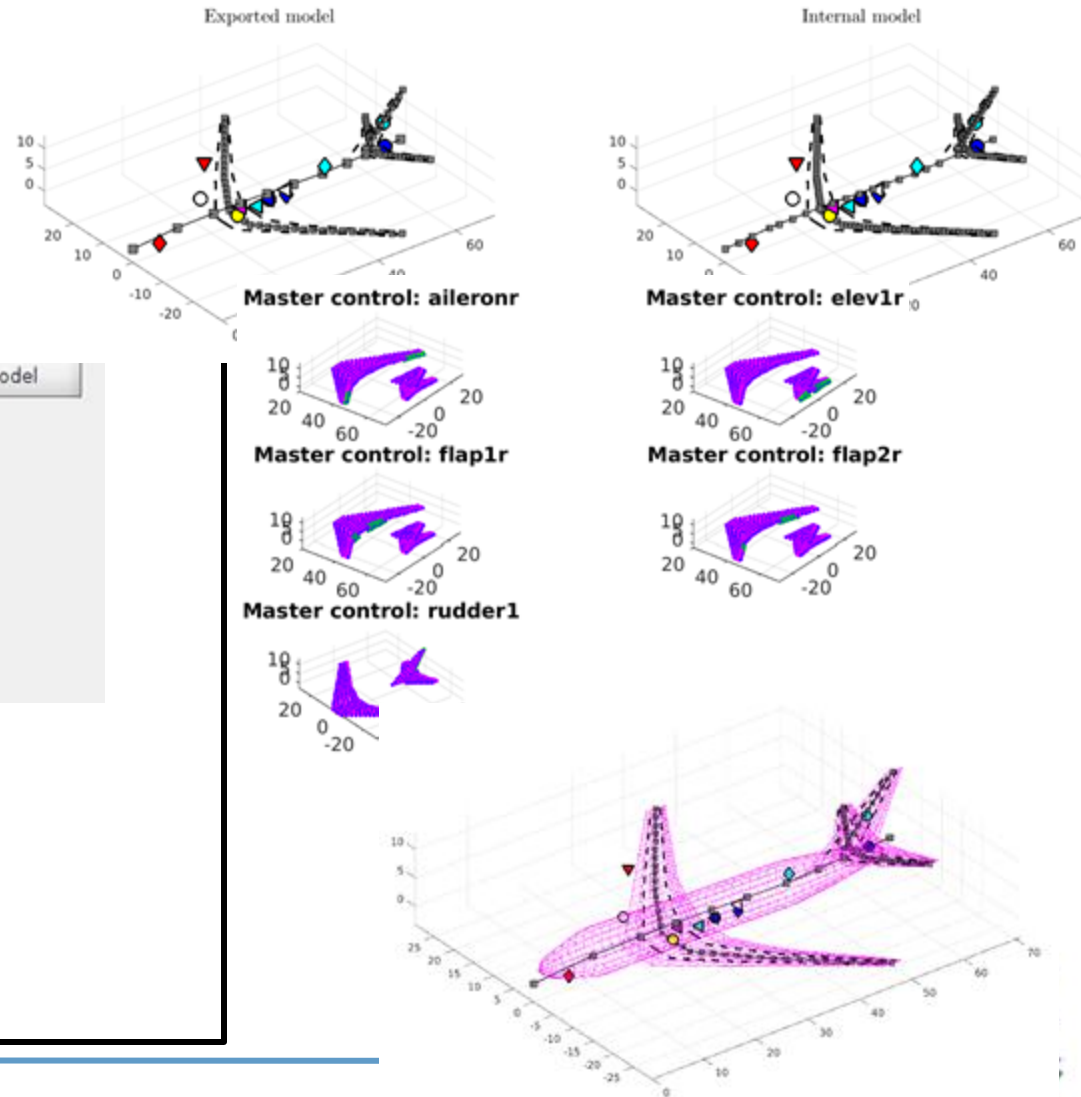
Model generation (5)

GUI

These buttons allows the visualization of the model

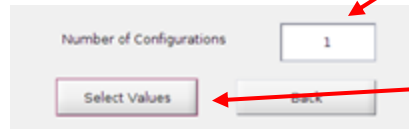


Run Mass Configuration



Model generation (6)

GUI



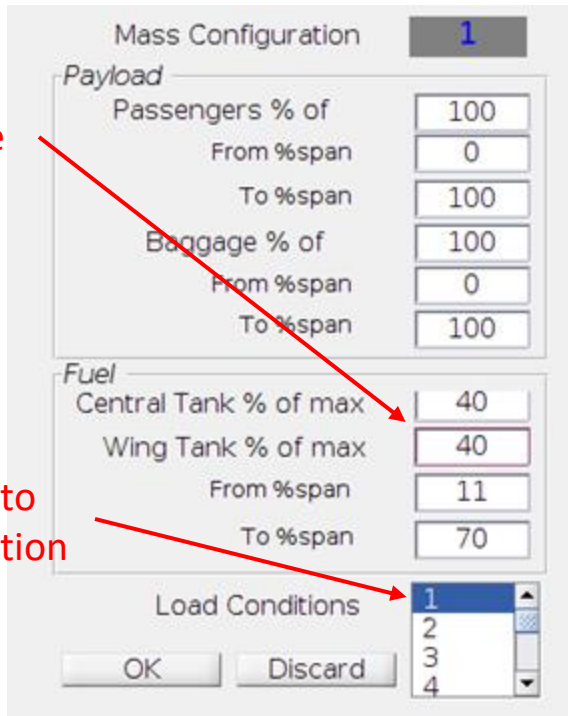
Number of Configurations: 1

Select Values

Specify 1 in the number of configurations defined

Press "Select values"

Define fuel quantity (set 40% of maximum value in wing and central tank)



Mass Configuration: 1

Payload

Passengers % of	100
From %span	0
To %span	100
Baggage % of	100
From %span	0
To %span	100

Fuel

Central Tank % of max	40
Wing Tank % of max	40
From %span	11
To %span	70

Load Conditions

- 1
- 2
- 3
- 4

OK Discard

Select all the trim conditions related to the mass configuration (select all)

Command line

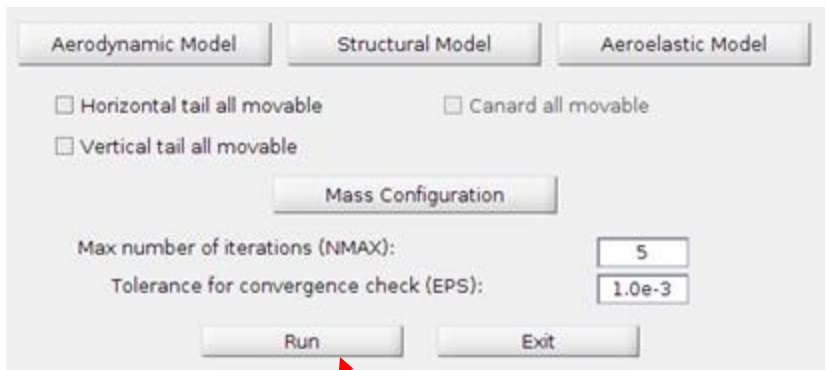
Define mass configurations (all fields are arrays for multiple mass configurations)

```
MassConf.Pass = 1;  
MassConf.Baggage = 1;  
MassConf.Cfuel = 0.4;  
MassConf.Wfuel = 0.4;  
MassConf.WfuelStart = 0;  
MassConf.WfuelArrive = []; % default from xml  
MassConf.WfuelStart = []; % default from xml  
MassConf.BagArrive = 1;  
MassConf.BagStart = 0;  
MassConf.PaxArrive = 1;  
MassConf.PaxStart = 0;  
MassConf.Load = []; % all maneuvers
```



Model generation (7)

GUI



Run GUESS

Command line

Set options (otherwise defaults values are used)

```
global NMAX EPS  
NMAX = 5;  
EPS = 0.001;
```

Initialize data structures

```
init_gui_params('neocass_gui_param.mat');  
init_guess_model;
```

Run GUESS

```
guess_model = guess(filename_geo,  
filename_tech, filename_stick, filename_trim,  
model, inBatch, MassConf);
```



Model generation (7)

Once the optimization is done, these files are generated

- B747-100 v00.inc : model data in Smartcad format

```
$  
$ Summary for total structural masses (CT included except for tailbooms):  
$ Wing: 78415.9373 Kg  
$ Htail: 4472.9978 Kg  
$ Vtail: 3164.1663 Kg  
$ Fuselage: 27537.1356 Kg  
$ Canard: 0 Kg  
$ Tailbooms: 0 Kg  
$  
$ Summary for secondary masses along fuselage (as PBAR density):  
$ Systems: 44985.7794 Kg  
$ Interior: 22000 Kg  
$ Pilots: 255 Kg  
$ Crew: 750 Kg  
$ Paint: 317.7345 Kg
```

- B747-100_v00CONM_CONF1.inc : masses for the defined configuration

```
$ Mass Configuration 1  
$ Baggage: 100% (4099.64 Kg)  
$ Passengers: 100% (41004.988 Kg)  
$ Wing Fuel: 40% (46000 Kg)  
$ Central Fuel: 40% (18400 Kg)
```

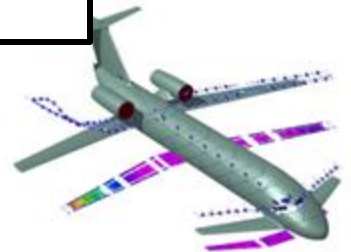


Import the model in Matlab (1)

The smartcad model can be imported in matlab, it is convenient to define a complete aeroelastic solver in order to enable all the portions of the code.

Here a static aeroelastic solution is used:

```
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
$ DATA ADDED AFTER GUESS SIZING
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
$ ADD PAYLOAD
INCLUDE B747-100_v00CONM_CONF1.inc
$-----2-----3-----4-----5-----6-----7-----8-----9-----10$
SET TRIM SOLVER
SOL 144
AEROS          0          10.483  59.64   551      0      0
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
$ ADD MANEUVERS
INCLUDE B747-100_CAS25.inc
$
$ INCLUDE MODEL
INCLUDE B747-100_v00.inc
$
```



Import the model in Matlab (2)

The `load_nastran_model` command can be used to generate the `beam_model` data structure

```
global beam_model
filename_sma = 'inputMain_trim.dat';
beam_model = load_nastran_model(filename_sma);
plotNeoModel(beam_model);
```

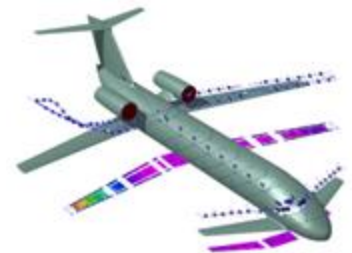


Import the model in Matlab (3)

```
>> beam_model
beam_model =
  Info: [1x1 struct]
  Param: [1x1 struct]
  Coord: [1x1 struct]
  Node: [1x1 struct]
  Mat: [1x1 struct]
  Bar: [1x1 struct]
  PBar: [1x1 struct]
  Beam: [1x1 struct]
  PBeam: [1x1 struct]
  F: [1x1 struct]
  M: [1x1 struct]
  F_FLW: [1x1 struct]
  ConM: [1x1 struct]
  WB: [1x1 struct]
  SPC: [1x1 struct]
  Aero: [1x1 struct]
  Optim: [1x1 struct]
  Celas: [1x1 struct]
  RBE2: [1x1 struct]
  Gust: [1x1 struct]
  SET: [1x1 struct]
  Surfdef: [1x1 struct]
  Dextload: [1x1 struct]
  Damp: [1x1 struct]
  DesOPT: [1x1 struct]
  Res: []
```

The beam_model structure contains all the data defining

- The structural model
- The aerodynamic model
- The solver and the solver parameters
- (after running a NeoCASS solver) the solver results



Import the model in Matlab (4)

```
>> beam_model.Bar
    ID: [1x82 double] ← Bar element IDs
    PID: [1x82 double]
    Conn: [82x3 double] ← Connectivity: position in Node database of the 3 bar nodes
    Orient: [82x3 double]
    OffsetT: [1x82 double]
    Offset: [82x9 double]
    Colloc: [2x3x82 double] ← Collocation points: coordinates of the points for load recovery
        R: [4-D double] ← Local orientation matrix (5 points: node1, colloc1, node2, colloc2, node3)
        D: [4-D double]
        M: [4-D double]
    barg0: [1x82 double]

>> beam_model.Node
    ID: [1x512 double] ← Node ID list
    CS: [1x512 double]
    Coord: [512x3 double] ← Node coordinates
    CD: [1x512 double]
    Index: [1x512 int32]
        R: [3x3x512 double] ← Node orientation matrix
        DOF: [512x6 int32] ← Table indicating for each nodal DOF the position in the global DOF vector
    Aero: [1x1 struct] ← Aeronodes associated to each structural node
    DOF2: [512x6 int32] ← As Node.DOF, but also RBE2 are considered in the definition of the global DOF
```

beam_model.Node.DOF : a zero value means that the corresponding DOF is constrained by a RBE0 or a SPC

beam_model.Node.DOF2 : a zero value means that the corresponding DOF is constrained by a RBE0, an SPC or a RBE2



Import the model in Matlab (5)

```
>> beam_model.Aero
```

```
    ID: [200 250 201 251 202 252 204 254 400 450 401 451 402 452 301 302 300]
```

```
    CP: [0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0]
```

```
    IS: [1x17 struct] ← Interpolation SETs
```

```
    INT: [0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0]
```

```
    AESURF: [1x1 struct]
```

```
    geo: [1x1 struct] ← Geometry of lifting surfaces  
        (with control surface definition)
```

```
    state: [1x1 struct]
```

```
    ref: [1x1 struct] ← Reference dimensions
```

```
    lattice: []
```

```
    lattice_defo: []
```

```
    lattice_vlm: [1x1 struct] ← Aerodynamic mesh for  
        VLM computation
```

```
    lattice_dlm: []
```

```
    Interp: [1x1 struct] ← Spline definition
```

```
    Set: [1x1 struct]
```

```
    Trim: [1x1 struct] ← Trim cases
```

```
    body: [1x1 struct] ← Aerodynamic mesh for  
        interference bodies
```



Export to NASTRAN model

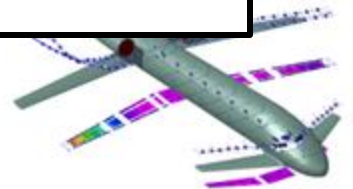
It is possible to export the model in NASTRAN format

- Only the model is exported, not the solver parameters
- It is necessary to define a complete aeroelastic solution input file for exporting the model

```
>> neo2nastran(inputFileName, outputFileName)
```

For example, using the input file with the static aeroelastic load definition:

```
filename_sma = 'inputMain_trim.dat';  
  
neo2nastran(filename_sma, 'B747-100_v00_Nastran.bdf')
```



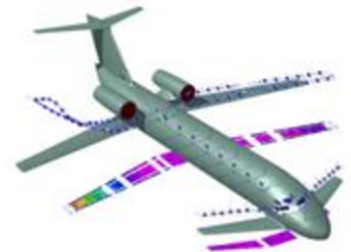
Aeroelastic static analysis (1)

NeoCASS can perform static trim and maneuver analysis

- Solution performed in mean axes
- Vortex Lattice Panel method used to compute aerodynamic forces

$$\begin{bmatrix} M_{rr} & M_{rd} \\ M_{dr} & M_{dd} \end{bmatrix} \begin{bmatrix} \ddot{u}_r \\ \ddot{u}_d \end{bmatrix} + \begin{bmatrix} \bar{K}_{rr} & \bar{K}_{rd} \\ \bar{K}_{dr} & \bar{K}_{dd} \end{bmatrix} \begin{bmatrix} u_r \\ u_d \end{bmatrix} = \begin{bmatrix} f_d \\ f_r \end{bmatrix} + q_\infty \begin{bmatrix} K_d^a \\ K_r^a \end{bmatrix} x_a$$

- u_r : rigid motion
 - u_d : structural deformations
 - M : mass matrix
 - K : Stiffness matrix (structural and aerodynamic)
 - f : external forces
 - x_a : aircraft attitude (α, β, p, q, r)
- Computes:
 - Aerodynamic coefficients (corrected)
 - Trim solution
 - Structural deformations
 - Aerodynamic loads
 - Internal forces



Aeroelastic static analysis (2)

- The stiffness matrix already includes aerodynamic contribution

$$\bar{\mathbf{K}}_{zz} = \mathbf{K}_{zz} - q_{\infty} \mathbf{K}_{zz}^a$$

- Inertial forces from deformable motion neglected, rigid displacement assumed null (fixed axes/mean axes)

$$\begin{bmatrix} \mathbf{M}_{dt} \\ \mathbf{M}_{tt} \end{bmatrix} \ddot{\mathbf{u}}_t + \begin{bmatrix} \bar{\mathbf{K}}_{dd} & \bar{\mathbf{K}}_{dt} \\ \bar{\mathbf{K}}_{td} & \bar{\mathbf{K}}_{tt} \end{bmatrix} \begin{bmatrix} \mathbf{u}_d \\ \mathbf{u}_t \end{bmatrix} = \begin{bmatrix} \bar{\mathbf{F}}_d \\ \bar{\mathbf{F}}_t \end{bmatrix} + q_{\infty} \begin{bmatrix} \mathbf{K}_{du}^a \\ \mathbf{K}_{tu}^a \end{bmatrix} \mathbf{v}_b + q_{\infty} \begin{bmatrix} \mathbf{K}_{dc}^a \\ \mathbf{K}_{tc}^a \end{bmatrix} \delta_c$$

The trim equations including aeroelastic effects are then solved as

$$\tilde{\mathbf{M}}_{tt} \ddot{\mathbf{u}}_t = \tilde{\mathbf{F}}_t^{ext} + \tilde{\mathbf{F}}_{0t}^a + q_{\infty} \tilde{\mathbf{K}}_{tu}^a \mathbf{v}_b + q_{\infty} \tilde{\mathbf{K}}_{tc}^a \delta_c$$



Aeroelastic static analysis (3)

$$\tilde{\mathbf{M}}_{tt}\ddot{\mathbf{u}}_t = \tilde{\mathbf{F}}_t^{ext} + \tilde{\mathbf{F}}_{0t}^a + q_\infty \tilde{\mathbf{K}}_{tu}^a \mathbf{v}_b + q_\infty \tilde{\mathbf{K}}_{tc}^a \delta_c$$

The equation components are defined by the user through the TRIM and SUPORT cards

- TRIM card defines values for

Flight condition	Mach, q_∞
URDD1, URDD2, ...	$\ddot{\mathbf{u}}_t$
ALPHA, BETA, ROLL, PITCH, YAW	\mathbf{v}_b
Control surfaces	δ_c

- The SUPORT card is used to define the rigid motion



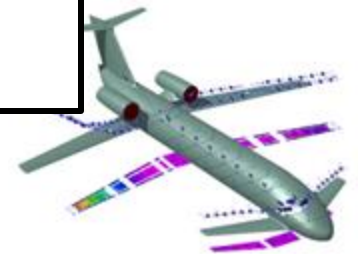
Aeroelastic static analysis example (1)

Definition of the Smartcad input file (`inputMain_trim.inc`)

```
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
$ DATA ADDED AFTER GUESS SIZING
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
$ ADD PAYLOAD
INCLUDE B747-100_v00CONM_CONF1.inc
$-----2-----3-----4-----5-----6-----7-----8-----9-----10$
SET TRIM SOLVER
SOL 144
AEROS          0          10.483  59.64   551      0          0
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
$ ADD MANEUVERS
INCLUDE B747-100_CAS25.inc
$
$ INCLUDE MODEL
INCLUDE B747-100_v00.inc
$
```

Trim condition definition (`B747-100_CAS25.inc`)

```
TRIM= 1
TRIM  1          1          0.5232360.0    SIDES  0.0    ROLL  0.0
      PITCH  0.0    YAW    0.0    URDD2  0.0    THRUST 0.0
      URDD4  0.0    URDD5  0.0    URDD6  0.0    CLIMB  0.0
      BANK  0.0    HEAD  0.0    URDD3  24.525  aileronr0
      flap1r 0      flap2r 0      rudder1 0
```



Aeroelastic static analysis example (2)

Performs a trim analysis using the configuration with ID 1:

```
global beam_model
filename_sma = 'inputMain_trim.dat';
beam_model = load_nastran_model(filename_sma);
solve_free_lin_trim('INDEX', 1);
plotLinearDispl(beam_model, beam_model.Res, 1, 1);
```

Solution available as

- `beam_model.Res` data structure
- text file (`inputMain_trim_man_1.txt`)



Aeroelastic static analysis example (3)

beam_model.Res data structure

```
>> beam_model.Res  
ans =
```

```
SOL: 'Static linear unrestrained trim'  
FM: [1x1 struct]  
CS: [1x1 struct]  
state: [1x1 struct]  
Bar: [1x1 struct]  
Beam: [1x1 struct]  
NDispl: [512x6 double]  
NRd: [3x3x512 double]  
Aero: [1x1 struct]  
Struct: [1x1 struct]  
CPaero: [1x1 struct]  
Trim: [1x1 struct]  
WB: [1x1 struct]
```

Internal forces on bars (described later)

```
CForces: [2x6x82 double]  
CStrains: [2x6x82 double]  
CStresses: [1x1 struct]  
CSM: [1x1 struct]  
R: [4-D double]  
Colloc: [2x3x82 double]
```

Node displacement

Structural matrices M and K (described later)

Aerodynamic forces/coefficients on aerodynamic mesh

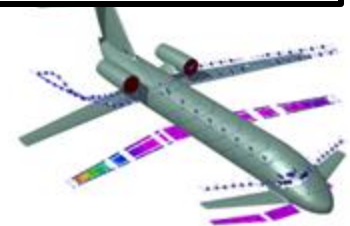
```
State: [1374x5 double]  
Control: [1374x5 double]  
Defo: [1374x1008 double]  
F0: [458x3 double]
```

Aerodynamic forces/coefficients

```
RStab_Der: [1x1 struct]  
RIntercept: [1x1 struct]  
DStab_Der: [1x1 struct]  
DIntercept: [1x1 struct]  
RTrim_sol: [1x1 struct]  
DTrim_sol: [1x1 struct]  
Qaa: [988x988 double]  
Kax: [988x10 double]  
QaaDOF: [1008x1008 double]  
KaxDOF: [1008x10 double]  
Fa0: [988x1 double]  
Fa0DOF: [1008x1 double]  
H: [5x10 double]  
H0: [5x1 double]  
DIVERG_Q: 0  
Fa0tot: [1008x2 double]  
XYZ: [458x3 double]  
F0_RTrim: [458x3 double]  
F0_DTrim: [458x3 double]  
RStability: [1x1 struct]  
DStability: [1x1 struct]
```

Trim condition definition

Mass distribution of the aircraft



Aeroelastic static analysis (4)

- text file (`inputMain_trim_man_1.txt`)

ELASTIC TRIM RESULTS

```
- X acc:      -6.95218e-13 [m/s^2].
- Y acc:      0 [m/s^2].
- Z acc:      24.525 [m/s^2].
- P-DOT:     0 [rad/s^2].
- Q-DOT:     0 [rad/s^2].
- R-DOT:     0 [rad/s^2].
- Alpha:     8.46657 [deg].
- Sideslip:  0 [deg].
- Roll rate:  0 [-] (p*BREF/(2VREF)).
- Pitch rate: 0 [-] (q*CREF/(2VREF)).
- Yaw rate:  0 [-] (r*BREF/(2VREF)).
- Control flap1r: 0 [deg].
- Control flap2r: 0 [deg].
- Control aileronr: 0 [deg].
- Control elev1r: 12.3955 [deg].
- Control rudder1: 0 [deg].
```

AERODYNAMIC DERIVATIVES

ALPHA

NAME	RIGID	ELASTIC	RATIO E/R
Cy/alpha	-0.00000	0.00000	-0.43068
Cz/alpha	3.97805	3.62291	0.91072
Cl/alpha	0.00000	-0.00000	-204.05294
Cm/alpha	-0.34431	-0.24801	0.72031
Cn/alpha	-0.00000	0.00000	-0.11343

BETA

NAME	RIGID	ELASTIC	RATIO E/R
Cy/beta	0.43077	0.40741	0.94579
Cz/beta	-0.00000	-0.00000	0.85057
Cl/beta	-0.13204	-0.12380	0.93760
Cm/beta	-0.00000	-0.00000	0.95816
Cn/beta	0.07728	0.06671	0.86320

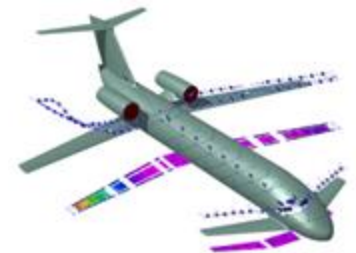
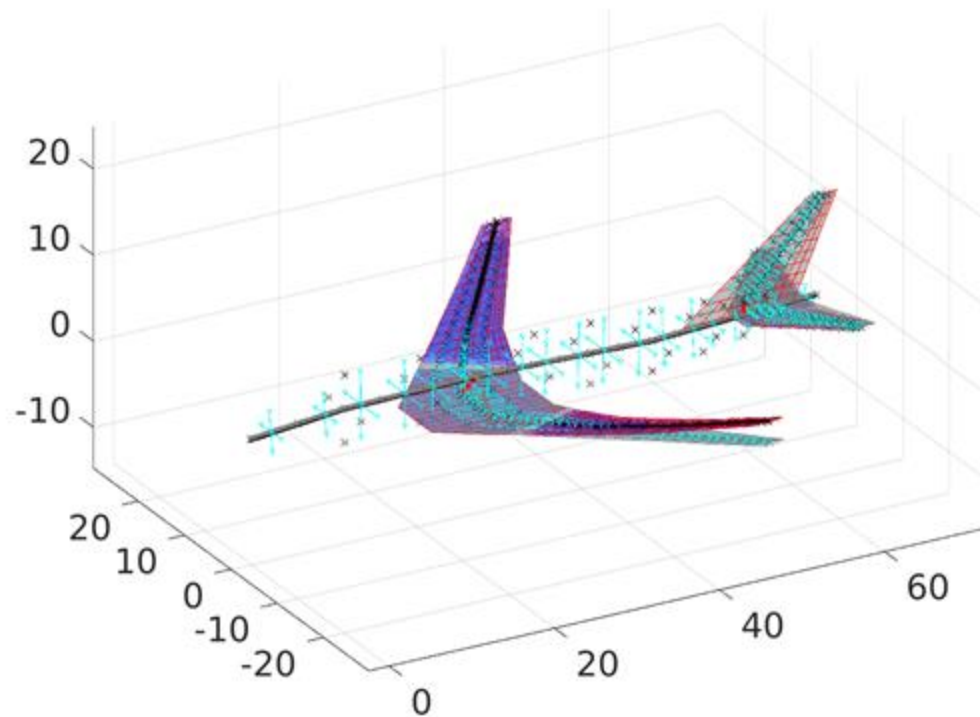


Aeroelastic static analysis (5)

Display the deformed aircraft

```
plotLinearDispl (beam_model, beam_model.Res, 1, 1);
```

Trim solution 1



Aeroelastic static analysis - recover nodal load (1)

The internal forces on bars are defined in beam_model.Res.Bar struct

```
>> beam_model.Res.Bar
ans =
    CForces: [2x6x82 double]
    CStrains: [2x6x82 double]
    CStresses: [1x1 struct]
        CSM: [1x1 struct]
        R: [4-D double]
    Colloc: [2x3x82 double]
```

Internal forces stored as

Loads on the structural nodes, for each bar, on the evaluation points.

beam_model.Res.Bar.CForces [2x6xnumberOfBars]

Coordinates of the points for load recovery

beam_model.Bar.Colloc [2 x 3 x numberOfBars]

Example of load recovery procedure:

```
% Get position of bar in dataset from element ID
barID = 2001;
position = beam_model.Bar.ID==barID;

% Forces on the first recovery point of the bar (in the bar reference system)
barForces = beam_model.Res.Bar.Cforces(1,:,position);

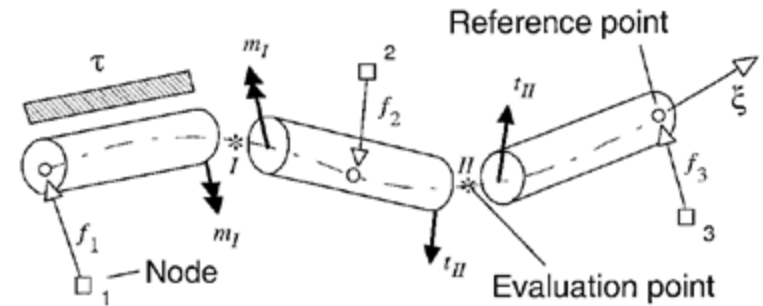
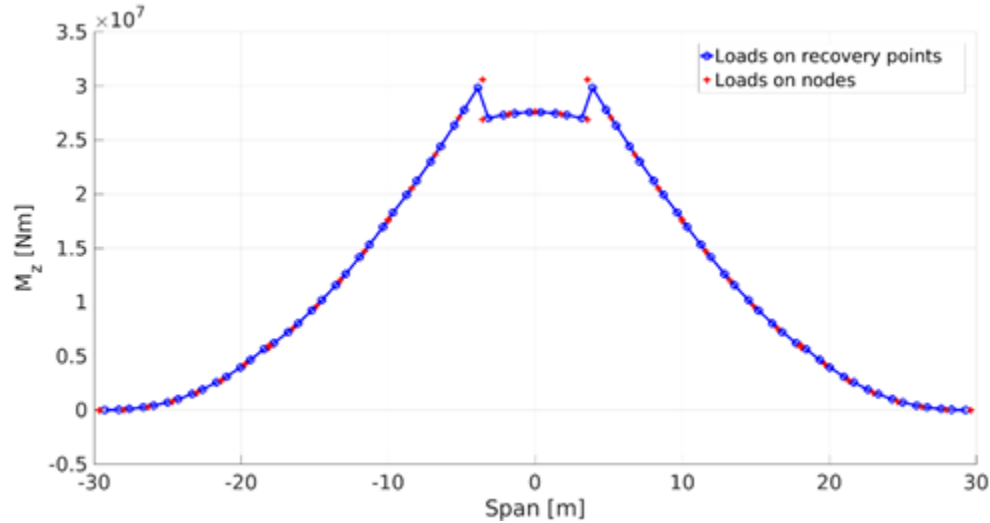
% Rotate forces in the basic reference system
R = beam_model.Bar.R(:, :, 2, position);
barForces_basic = [R*barForces(1:3)'; R*barForces(4:6)'];

% Get the coordinates of the evaluation point
pointCoord = beam_model.Bar.Colloc(1,:,position);
```



Aeroelastic static analysis - recover nodal load (2)

The internal forces on bars are defined in the load evaluation points. It is possible to obtain them in the beam nodes

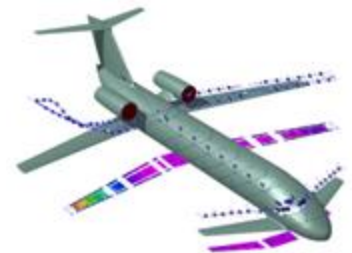


The load transfer can be performed using the `getForcesOnNodes` function

```
[NForces, nodeCoords] = getForcesOnNodes (beam_model, beam_model.Res.Bar.CForces);
```

NForces [2 x 6 x numberOfBars]: loads on the structural nodes, for each bar.

NodeCoords [2 x 3 x numberOfBars]: coordinates of the nodes used for load recovery.



Recover structural matrices

Mass and stiffness matrices can be recovered from `beam_model.Res.Struct`

```
>> beam_model.Res.Struct
      M: [988x988 double]
      K: [988x988 double]
      F: [988x1 double]
      D: [982x6 double]
      ldof: [1x982 double]
      rdof: [25 26 27 28 29 30]
```

The matrices contain only the free DOFs

- Without considering the aeronodes
- Including the mid-bar nodes
- Without DOFs constrained by RBE2 and SPC

The correspondence DOF – position in matrices can be obtained as

```
beam_model.Node.DOF2(iNode,iComponent)
```

This gives the position of the component `iComponent` of node `iNode`, if it is zero the component is constrained (RBE0, RBE2, SPC)



Divergence analysis example (1)

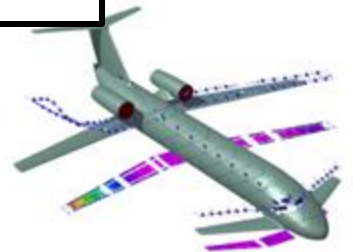
Divergence dynamic pressure computed by solving an eigenvalue problem

$$\det \left(\tilde{\mathbf{K}}_{dd} - \lambda \tilde{\mathbf{K}}_{dd}^a \right) = 0$$

- The lowest real, positive eigenvalue will provide the divergence dynamic pressure.
- The computation is performed using matrices in mean axes.

Definition of the Smartcad input file (`inputMain_diverg.inc`)

```
$  
PARAM   DIVERG   1  
$  
$  
PARAM   CMOFUS  -0.01  
PARAM   CMAFUS   0.03  
  
[...]
```



Divergence analysis example (2)

Screen output →

```
>> beam_model.Res  
  
ans =  
  
  struct with fields:  
  
      SOL: 'Static linear unrestrained  
trim'  
  
      FM: [1x1 struct]  
      CS: [1x1 struct]  
      state: [1x1 struct]  
      Bar: [1x1 struct]  
      Beam: [1x1 struct]  
      NDispl: [512x6x2 double]  
      NRd: [3x3x512x2 double]  
      Aero: [1x1 struct]  
      Struct: [1x1 struct]  
      CPaero: [1x1 struct]  
      Trim: [1x1 struct]  
      WB: [1x1 struct]
```

```
[...]  
  
- Control flap1r:  0 [deg].  
- Control flap2r:  0 [deg].  
- Control aileronr:  0 [deg].  
- Control elev1r:  7.43586 [deg].  
- Control rudder1:  0 [deg].  
done.  
Solving for unrestrained aeroelastic divergence...  
- Divergence dynamic pressure: 5.084410e+06 [Pa].  
done.  
- Updating vlm model in Aero.lattice_defo...done.  
[...]
```

← Results Structure

Deformation associated to divergence mode



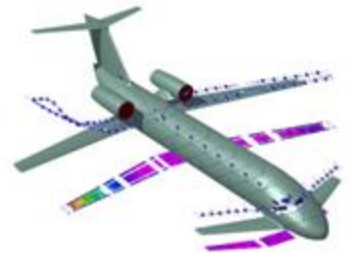
Specification of fuselage moment coefficients (1)

It is possible to directly provide the fuselage $C_{m\alpha}$ coefficients

- The provided value is not used in the aerodynamic or structural computations
- The provided value is only used in the computation of the displayed static margin

Definition of the Smartcad input file (`inputMain_diverg.inc`)

```
[...]  
PARAM CMAFUS 0.03  
[...]
```



Specification of fuselage moment coefficients (2)

Results file without Cma definition (`inputMain_man_1.txt`)

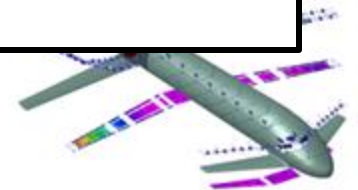
```
STABILITY

NAME                                RIGID                                ELASTIC
Center of gravity                    XG/CREF                             3.20550
Neutral point at fixed stick XN/CREF 3.15124                             3.10956
Control point at fixed stick XC/CREF 6.10821                             5.77632
Static margin      (XN-XCG)/CREF    -0.05427                             -0.09594
Static margin index (XN-XCG)/(XC-XN) -0.01835                             -0.03598
```

Results file with Cma definition (`inputMain_diverg_1.txt`)

```
STABILITY

NAME                                RIGID                                ELASTIC
Center of gravity                    XG/CREF                             3.20550
Neutral point at fixed stick XN/CREF 3.34434                             3.32028
Control point at fixed stick XC/CREF 6.10821                             5.77632
Static margin      (XN-XCG)/CREF    0.13884                             0.11477
Static margin index (XN-XCG)/(XC-XN) 0.05023                             0.04673
```



Modification of aerodynamic forces with external data

Linear aerodynamic forces:

$$\frac{\mathbf{F}_z^a}{q_\infty} = \mathbf{F}_0^a + \mathbf{K}_u^a \mathbf{v}_b + \mathbf{K}_c^a \boldsymbol{\delta}_c + \mathbf{K}_z^a \mathbf{u}_z$$

Aerodynamic forces on structural DOFs

Structural DOFs

By default all the components are obtained using the VLM method.

There is the possibility to:

- Provide directly \mathbf{F}_0^a
- Provide directly columns of \mathbf{K}_c^a and \mathbf{K}_u^a
- Provide scaling factors for \mathbf{K}_c^a and \mathbf{K}_u^a



Modification of aerodynamic forces with external data

Definition of steady forces

The following files are used in this portion of the tutorial:

- `inputMain_trimExtType2.dat` : Smartcad input file
- `exampleMain_trimExtType2.m` : Matlab script

Definition of the Smartcad input file (`inputMain_trimExtType2.dat`)

- The TRIMEXT entry can be used to introduce additional aerodynamic components, with the aerodynamic loads
- Several entries can be defined specifying each component (wing, fuselage etc...)
- A beam spline is used to connect the aerodynamic mesh to the structural mesh

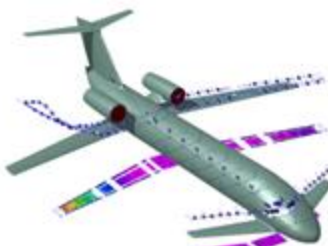
```
$
$-----2-----3-----4-----5-----6-----7-----8-----9-----
TRIMEXT 100      './CFDresults/wing-right_base.bdf'
          1      0      0      210
          201    202    203
[...]
```

File with the mesh and load definition (see `CFDresults/wing-right_base.bdf`)

ID of SET entry for spline definition (210)

Position and reference system (0 0 210)

CAEROs that will be substituted by the imported elements (201 202 203)



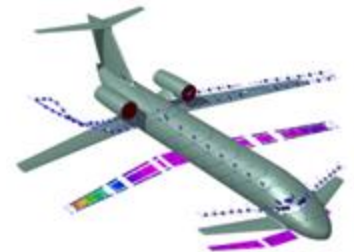
Modification of aerodynamic forces with external data

Definition of the Imported mesh file (CFDresults/wing-right_base.bdf)

The mesh file contains

- the imported nodes
- the elements
- the pressure coefficients on each element

```
$
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
GRID      1100001 0          48.4992 29.5977 1.21137 0
[... ]
CTRIA3    1100001 0 1100001 1100002 1100003
[... ]
PLOAD4    1000      1109614 -1.089
[... ]
```



Modification of aerodynamic forces with external data

Definition of force derivatives (substitution of columns)

- Forces are obtained by finite differences, defining the value for perturbed ALPHA, BETA, ... and subtracting the value at the reference condition
- This correction is enabled by the **PARAM DER_TYPE=2**

Definition of the Smartcad input file (inputMaing_trimExtType2.dat)

```
PARAM DER_TYPE 2
$-----2-----3-----4-----5-----6-----7-----8-----
TRIMEXT 100 './CFDresults/wing-right_base.bdf'
      1 0 0 1100 210
      201 202 204
$-----2-----3-----4-----5-----6-----7-----8-----
DEREXT 1100
      ALPHA 0.0349 './CFDresults/wing-right_alpha.bdf'
$
[ ]
```

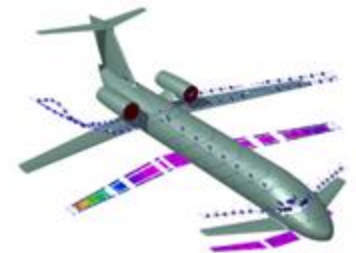
ID of DEREXT card defining the CFD results in perturbed condition

Several lines like this can be repeated for each DEREXT entry

Perturbed variable

Value of perturbed variable

File with results in perturbed conditions



Modification of aerodynamic forces with external data

Modification of force derivatives (scaling of columns)

- Forces are obtained by scaling a whole column of matrices
- This correction is enabled by the `PARAM DER_TYPE=1`

Definition of the Smartcad input file (`inputMain_trimExtType1.dat`)

```
PARAM DER_TYPE 1
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
TRIMEXT 100 './CFDresults/wing-right_base.bdf'
        1 0 0 210
        201 202 204
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
PARAM DER_FILE './CFDresults/correctionFactors.bdf'
$
[...]
```

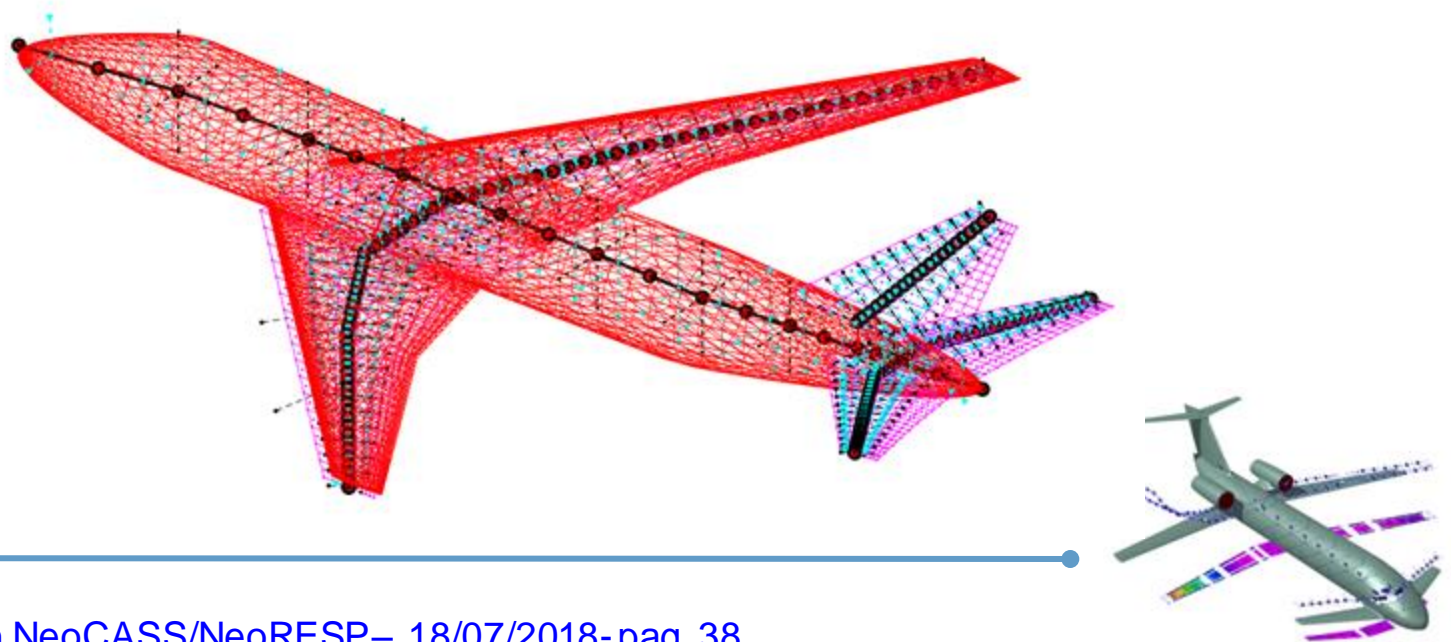
File with scaling factors

```
alpha 0.90
elev1r 0.8
```



Modification of aerodynamic forces with external data

- Also a partial substitution of aerodynamic surfaces can be performed.
- The VLM computation will always be performed considering all the CAEROs to get the correct aerodynamic interference.
- The forces generated by the substituted CAEROs will be discarded



Modal / flutter analysis (1)

The aeroelastic module in NeoCASS can perform

- Modal analysis on the structure defined on the Smartcad input file
- Import modal basis obtained from an external solver (not shown in this tutorial)
- Compute unsteady aerodynamic generalized forces in frequency domain based on the Doublet Lattice Method.
- Compute the roots of the aeroelastic system in a velocity range, using a continuation method.

The following files are used in this portion of the tutorial:

- `inputMain_flutter.dat` : Smartcad input file
- `exampleMain_flutter.m` : Matlab script



Modal / flutter analysis (2)

Aeroelastic system equations in frequency domain:

$$[\mathbf{M}s^2 + \mathbf{C}s + \mathbf{K} - q_\infty(v)\mathbf{H}_{\text{am}}(p(s), M_\infty(v))] \mathbf{q} = 0$$

Aerodynamic matrices from DLM → \mathbf{H}_{am}
Modal displacement → \mathbf{q}
Laplace variable → s
Reduced frequency → v
Modal (structural) mass, damping and stiffness → $\mathbf{M}, \mathbf{C}, \mathbf{K}$

Compact form: $\mathbf{F}(s, v)\mathbf{q} = 0$

The flutter eigenvalue and mode are found by solving a system of ODE on the flight speed

$$\begin{bmatrix} \frac{\partial \mathbf{F}(s, v)}{\partial s} & \mathbf{F}(s, v) \\ 0 & \mathbf{q}^H \end{bmatrix} \begin{bmatrix} \frac{ds}{dv} \\ \frac{d\mathbf{q}}{dv} \end{bmatrix} = \begin{bmatrix} -\frac{\partial \mathbf{F}(s, v)}{\partial v} \\ 0 \end{bmatrix}$$



Modal / flutter analysis example (1)

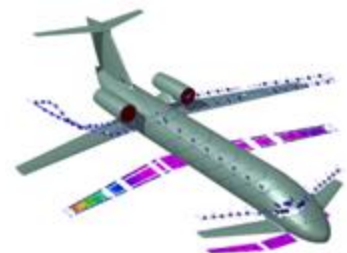
Smartcad input file (`inputMain_flutter.dat`)

Compute the first 20 modes with frequency lower than 300Hz

```
[...]
SOL 145
$ Eigenvalue solver parameters
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
EIGR    1              0              300              20              MASS
$ Doublet lattice solver parameters
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
AERO    551          300          10.483  1.225  0          0          2          100          59.64
$ Doublet lattice aerodynamic transfer matrix points
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
MKAERO1 0.50
          0.0005  0.001  0.002  0.005  0.01  0.05  0.1  0.2
MKAERO1 0.50
          0.5    1      1.5    2
$ Selected modes defining the modal basis
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
MSELECT  ← 1          2          3          4
           9          10         11         12
           17         18         19         20
$ Selected modes for tracking in V-g plot
$-----2-----3-----4-----5-----6-----7-----8-----9-----10
FMODES   7          8          9          10         11         12         13         14
           15         16         17         18         19         20
UMODES   1          2          3          4          5          6          7          8
           9          10         11         12         13         14         15         16
           17         18         19         20
```

Define aerodynamic data, including reference surface (551 m²) and reference span (59.64m)

Modes used to compute aerodynamic matrices



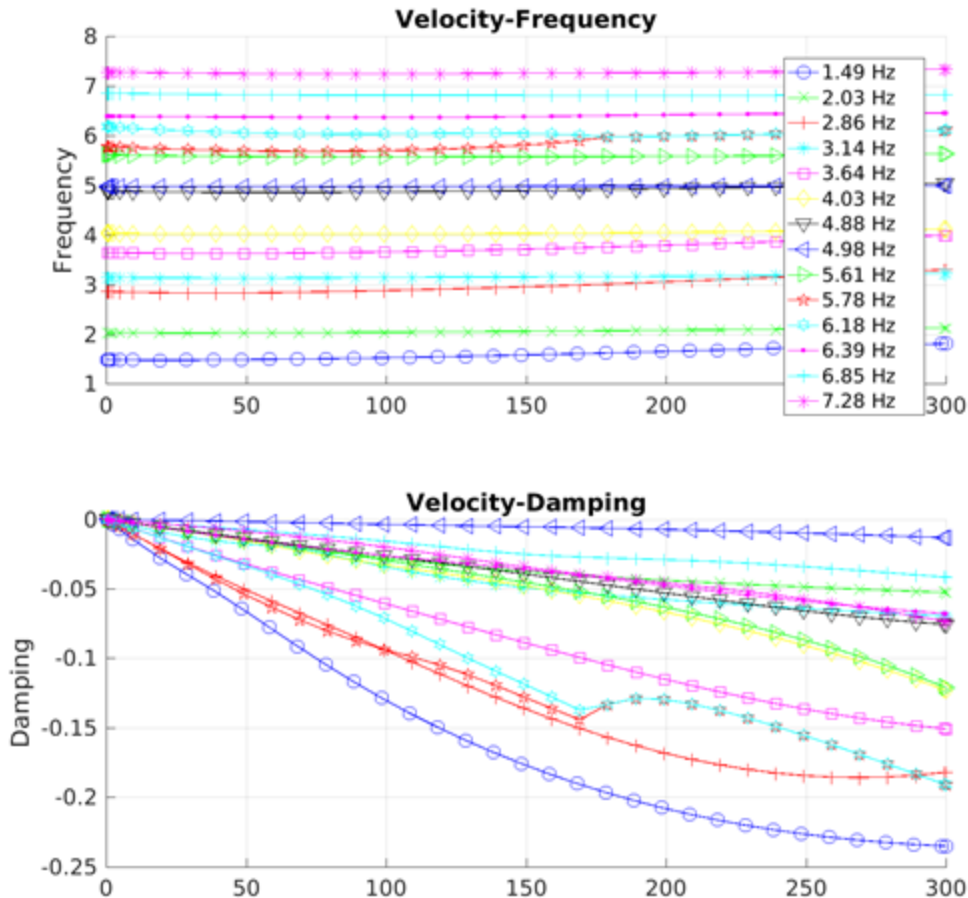
Modal / flutter analysis example (2)

Matlab script `exampleMain_flutter.m`

```
global beam_model  
  
filename_sma = 'inputMain_flutter.dat';  
  
beam_model = load_nastran_model(filename_sma);  
  
solve_linflutt();
```



Modal / flutter analysis example (3)



Results

```
global fl_model
```

```
fl_model
```

```
Res: [1x1 struct]
```

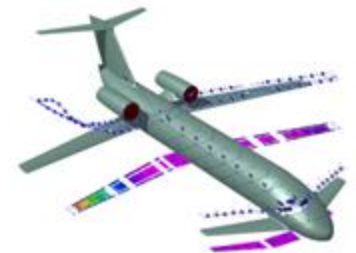
```
param: [1x1 struct]
```

```
ref: [1x1 struct]
```

```
struct: [1x1 struct]
```

```
interp: [1x1 struct]
```

```
aero: [1x1 struct]
```



Recover flutter results

```
global fl_model
>> fl_model.aero
ans =
    Qhh: [20x20x24 double]
    Mach: 0.5000
    Klist: [5.0000e-04 1.0000e-03 0.0020 0.0050 0.0100 0.0500 0.1000 0.2000
0.5000 1 1.5000 2]
    rho: 1.2250
```

Condensed aerodynamic matrix

```
>> fl_model.Res.data
ans =
```

```
    k: {1x14 cell}
Velocity: {1x14 cell}
    g: {1x14 cell}
    Freq: {1x14 cell}
    RealE: {1x14 cell}
    ImagE: {1x14 cell}
    g_Vder: {1x14 cell}
    F_Vder: {1x14 cell}
```

Velocities corresponding to the computed roots

Real/Imaginary part of the aeroelastic roots



Recover modal data

```
>> beam_model.Res
```

```
ans =
```

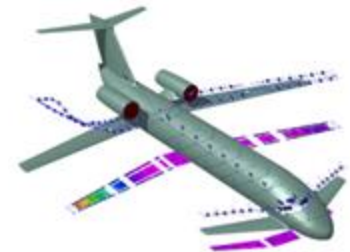
```
SOL: 'Linear flutter'  
NDispl: [512x6x20 double]  
NRd: [4-D double]  
Bar: [1x1 struct]  
Beam: [1x1 struct]  
Mmm: [20x20 double]  
Kmm: [20x20 double]  
M: [988x988 double]  
K: [988x988 double]  
Omega: [20x1 double]  
V: [988x20 double]  
ID: [1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20]
```

Nodal displacements on all structural nodes (modal matrix on all nodes)

Modal mass and stiffness matrices

Complete mass and stiffness matrices (defined as in the trim analysis)

Modal matrix on the free DOFs only



Dynamic response

NeoRESP is the module that can be used for dynamic response analysis, three types of analysis can be performed

- Gust response analysis
- Control surface deflection
- External forcing

The effects of the three types of forcing terms can be combined.

The computation is performed in frequency domain on a modally reduced system, with unsteady aerodynamic obtained using the DLM method



Dynamic response – input definition

In order to run NeoRESP is necessary to set

- The forcing term;
- The flight condition;
- The output of the simulation (displacements, loads, stresses ...)

In addition, also the data concerning the modal computation and the DLM aerodynamic matrix need to be set.

All the data can be defined in the input Smartcad file.



Simulation Parameters – forcing term

Gust input:

	Amplitude	Duration	Delay	Direction (vertical or horizontal gust)
GUST 1	17.07	0.12	0.0	3

$\sin(\pi * (x+25) / 50)$ ← Spanwise variation of the gust speed
 $(1 - \cos(2 * \pi / 0.1200 * t)) * 0.5$ ← Time evolution of the gust speed

Control surface deflection:

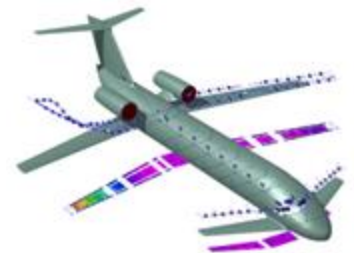
\$	ID	label	Amplit	TMAX	Delay
SURFDEF 1	1	elev1r	1.0	0.5	0.0

$\sin(2 * \pi / 0.5 * t)$

External load:

\$	ID	NODE	DOF	AMPLIT	TMAX	DELAY
DLOAD 1	1	2000	3	1.0e+3	0.5	0.0

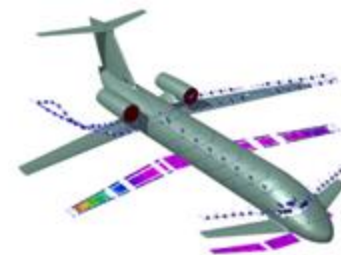
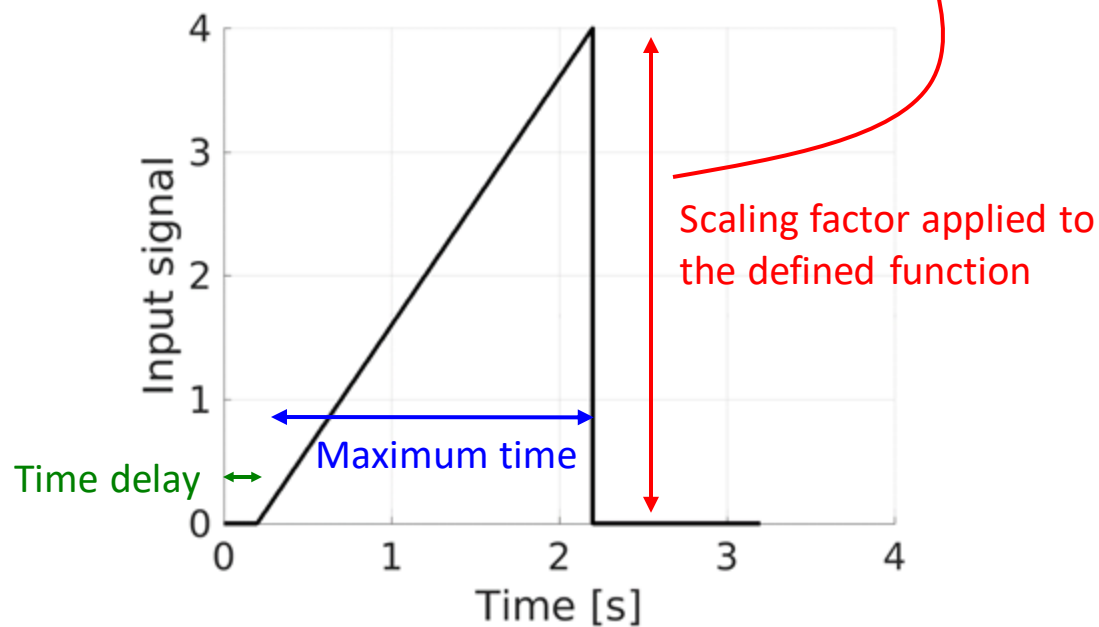
$\sin(2 * \pi / 0.5 * t)$



Simulation Parameters – forcing term

Example of input definition

\$	ID	NODE	DOF	AMPLIT	TMAX	DELAY
DLOAD	1	2000	3	1.0	2.2	0.2
	$2 * t$					



Simulation Parameters – forcing term

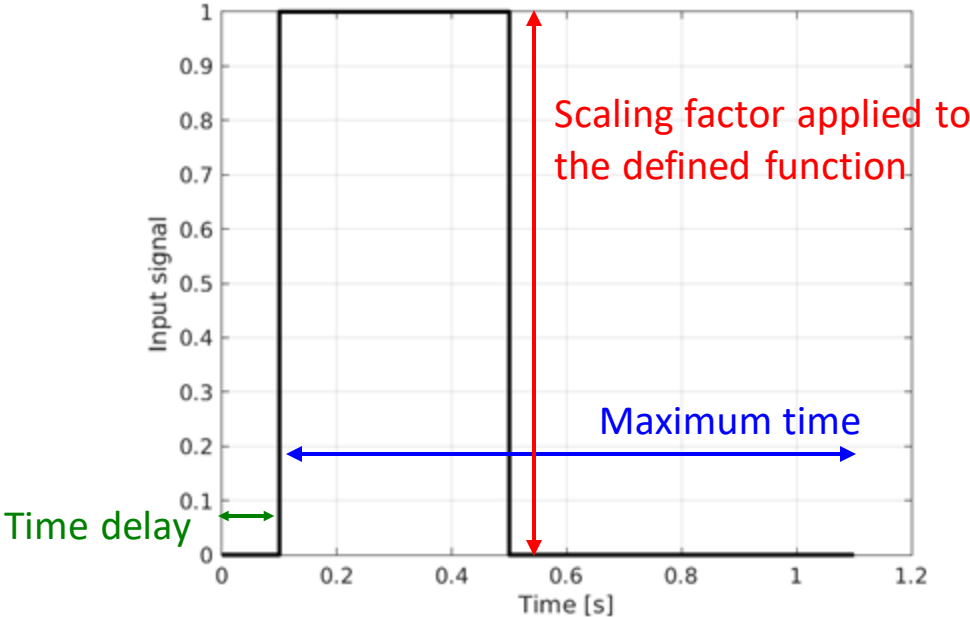
It is also possible to define the input through a list of points

```

$      ID      NODE  DOF  AMPLIT  TMAX  DELAY  TYPE
DLOAD  2      2020   3    1.0    1.0    0.1    TABLED
      4000
  
```

```

$
TABLED1      4000
             0.      1.      0.4      1.      0.4      0.      ENDT
  
```



Simulation Parameters – flight condition and output

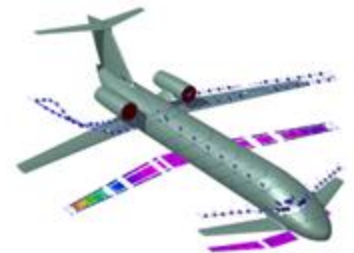
Flight condition:

PARAM	MODACC	0	← 0: Mode acceleration is active
PARAM	VREF	238.0	
PARAM	RHOREF	1.225	
PARAM	MACH	0.7	

Output selection:

SET 1 =	2002	4000	↙ Node/element sets
SET 2 =	2000		↘

DISP= ALL
ACCELERATION= 2
IFORCE= 1



Simulation results

The simulation results are stored in the `dyn_model.Res` data structure

An example of how to extract data from this structure is shown in the following examples.

```
dyn_model =  
  dlm: [1x1 struct]  
  beam: [1x1 struct]  
  flu: [1x1 struct]  
  gust: [1x1 struct]  
  Out: [1x1 struct]  
  Res: [1x1 struct]
```

Aerodynamic matrices

Model and results from modal analysis

Flutter results

Aerodynamic matrices associated with gust input

Simulation results



Simulation results

```
>> dyn_model.dlm.data
```

```
ans =
```

```
      D: [458x458x12 double]
      Cp: [458x25x12 double]
      Qhh: [20x20x12 double]
c_displ: [458x3x25 double]
dwnwash: [458x25x12 double]
n_displ: [1832x3x25 double]
  invD: [458x458x12 double]
  Qnh: [1008x20x12 double]
  Qhd: [20x5x12 double]
  Qdh: [5x20x12 double]
  Qdd: [5x5x12 double]
  Qnd: [1008x5x12 double]
  Hag: [20x1x12 double]
```

```
>> dyn_model.gust
```

```
ans =
```

```
dwnwash: [458x1 double]
      Cp: [458x458x12 double]
      Qhg: [20x458x12 double]
      Qng: [1008x458x12 double]
      Qdg: [5x458x12 double]
```

Aerodynamic matrices for
mode acceleration

Aerodynamic matrices from
control surface deflection



Gust response (1)

This example shows how to simulate a gust response of an aircraft

The following files are used in this portion of the tutorial:

- `inputMain_gust.dat` : Smartcad input file
- `exampleMain_gust.m` : Matlab script



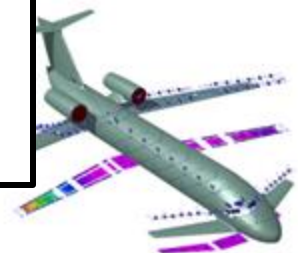
Gust response (2)

Smartcad input file

```
[...]  
SOL 146  
$  
PARAM      MODACC      0  
PARAM      VREF 170.000  
PARAM      RHOREF 1.22500  
PARAM      MACH 0.50000  
$-----2-----3-----4-----5-----6-----7-----8-----9-----10  
$ Output set (node list)  
$-----2-----3-----4-----5-----6-----7-----8-----9-----10  
SET 3 =      1004      2018  
SET 4 =      1004      2018  
$-----2-----3-----4-----5-----6-----7-----8-----9-----10  
$ Choose output (displacements, velocities, accelerations and internal forces)  
$-----2-----3-----4-----5-----6-----7-----8-----9-----10  
IFORCE= ALL  
DISP= ALL  
VELOCITY= 3  
ACCELERATION= 4  
HINGEFORCE= ALL  
$-----2-----3-----4-----5-----6-----7-----8-----9-----10  
GUST= 1  
$-----2-----3-----4-----5-----6-----7-----8-----9-----10  
$ Gust input  
$-----2-----3-----4-----5-----6-----7-----8-----9-----10  
GUST      1      17.07      0.40      0.0      3  
          1  
          (1-cos(2*pi/0.4000*t))*0.5
```

Enable load recovery with mode acceleration

Select the gust ID used in simulation



Gust response (3)

Matlab script

```
global beam_model
global dyn_model

filename_sma = 'inputMain_gust.dat';

init_dyn_model(filename_sma)

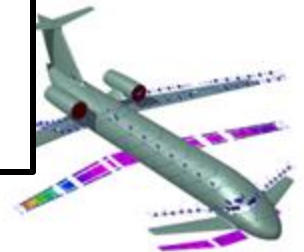
solve_free_lin_dyn('dT', 5e-3, 'Tmax', 6);

positionWR_global = find(beam_model.Bar.ID==2002);
positionWR_results = find(beam_model.Param.IFORCE==positionWR_global);

wrbm_dirrec = squeeze(dyn_model.Res.IFORCE(6,1,positionWR_results,:));
wrbm_modac = squeeze(dyn_model.Res.MODACC.IFORCE(6,1,positionWR_results,:));
wrtm_dirrec = squeeze(dyn_model.Res.IFORCE(4,1,positionWR_results,:));
wrtm_modac = squeeze(dyn_model.Res.MODACC.IFORCE(4,1,positionWR_results,:));
```

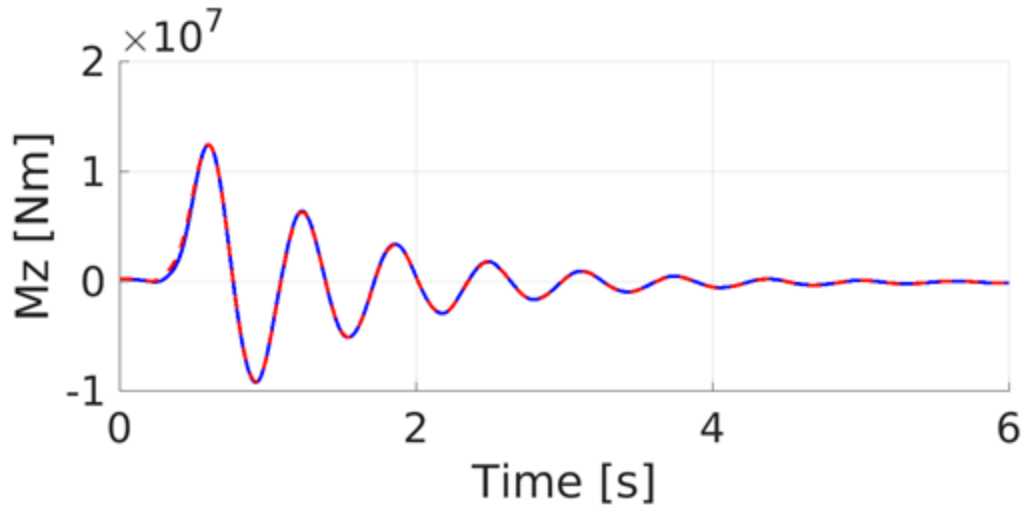
Define time step and duration

Extract loads from solution

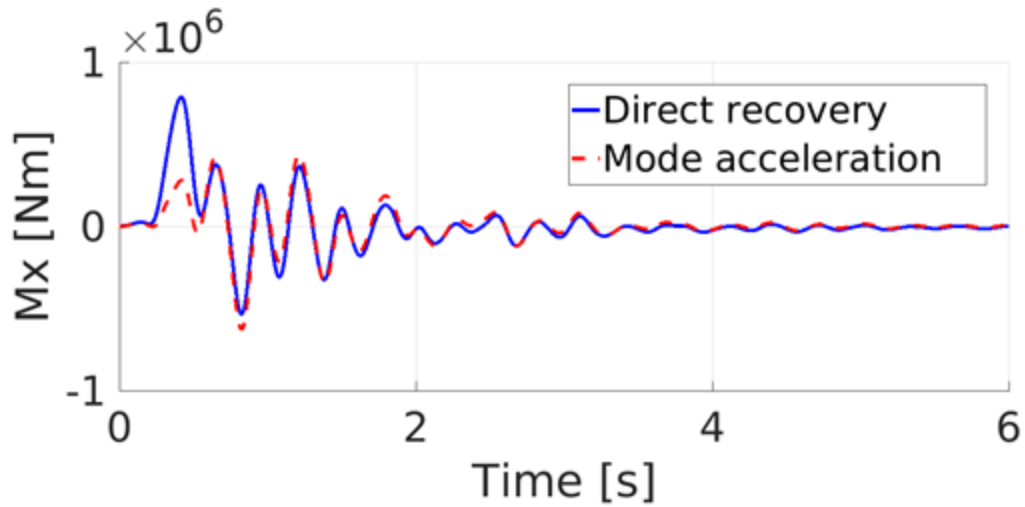


Gust response (4)

Wing root Bending moment



Wing root torsional moment



Gust response (5)

```
>> dyn_model.Res
  Gust_profile: [1x1201 double]
    Time: [1x1201 double]
    Qload: [20x1201 double]
    Qextf: [20x1201 double]
    Q: [20x1201 double]
    Qd: [20x1201 double]
    Qddot: [20x1201 double]
  Cy_mode: [1x1201 double]
  Cz_mode: [1x1201 double]
  Cl_mode: [1x1201 double]
  Cm_mode: [1x1201 double]
  Cn_mode: [1x1201 double]
  DISP: [512x6x1201 double]
  VELOCITY: [2x6x1201 double]
  ACCELERATION: [2x6x1201 double]
  IFORCE: [4-D double]
  HF_gust: [5x1201 double]
  HF_mode: [5x1201 double]
  Cy_gust: [1x1201 double]
  Cz_gust: [1x1201 double]
  Cl_gust: [1x1201 double]
  Cm_gust: [1x1201 double]
  Cn_gust: [1x1201 double]
  MODACC: [1x1 struct]
```

Modal coordinates and time derivatives

Outputs as required by the DISPLACEMENT=, VELOCITY= ... cards

Aerodynamic hinge moments divided by components
 $HF = HF_gust + HF_mode + HF_surf$
(HF_surf is not present here since no surface input is used)

Loads obtained with mode acceleration method

```
>> dyn_model.Res.MODACC
  IFORCE: [4-D double]
  DISP: [512x6x1201 double]
```



Gust response (6)

Recover output from a reduced output set.

Example of recovery of accelerations.

```
% Get position of node in dataset starting from node ID
nodeID = 2018;
position = find(beam_model.Node.ID==nodeID);

% Get the position of the node in the results dataset
positionInRespDISP = dyn_model.beam.Param.DISP==position;

% Get the time history (of the 6 components of displacements)
timeHistory = dyn_model.Res.DISP(positionInRespDISP,3,:);
```



Elevator deflection response (1)

This example shows how to simulate the response of an aircraft after the deflection of the elevator

The following files are used in this portion of the tutorial:

- `inputMain_cSurf.dat` : Smartcad input file
- `exampleMain_cSurf.m` : Matlab script



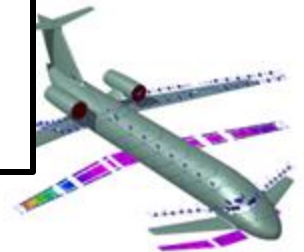
Elevator deflection response (2)

Smartcad input file

```
[...]  
SOL 146  
$  
PARAM      MODACC      0  
PARAM      VREF 170.000  
PARAM      RHOREF 1.22500  
PARAM      MACH 0.50000  
[...]  
$-----2-----3-----4-----5-----6-----7-----8-----9-----10  
SURFDEF= 2  
$-----2-----3-----4-----5-----6-----7-----  
$ Control surface input  
$-----2-----3-----4-----5-----6-----7-----  
SURFDEF 1      aileronr1.0      0.5      0.0  
                sin(2*pi/0.5*t)  
SURFDEF 2      elevlr 1.0      0.5      0.0  
                sin(2*pi/0.5*t)  
SURFDEF 3      rudder1 1.0      0.5      0.0  
                sin(2*pi/0.5*t)  
$
```

Enable load recovery with mode acceleration

Select the ID used in simulation among the IDs of the SURFDEF cards



Elevator deflection response (3)

Matlab script (no variation w.r.t. gust response!)

```
global beam_model
global dyn_model

filename_sma = 'inputMain_cSurf.dat';

init_dyn_model(filename_sma)

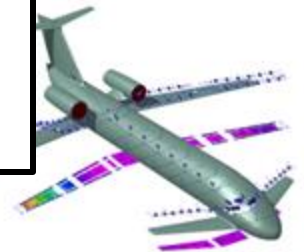
solve_free_lin_dyn('dT', 5e-3, 'Tmax', 6);

positionWR_global = find(beam_model.Bar.ID==2002);
positionWR_results = find(beam_model.Param.IFORCE==positionWR_global);

wrbm_dirrec = squeeze(dyn_model.Res.IFORCE(6,1,positionWR_results,:));
wrbm_modac = squeeze(dyn_model.Res.MODACC.IFORCE(6,1,positionWR_results,:));
wrtm_dirrec = squeeze(dyn_model.Res.IFORCE(4,1,positionWR_results,:));
wrtm_modac = squeeze(dyn_model.Res.MODACC.IFORCE(4,1,positionWR_results,:));
```

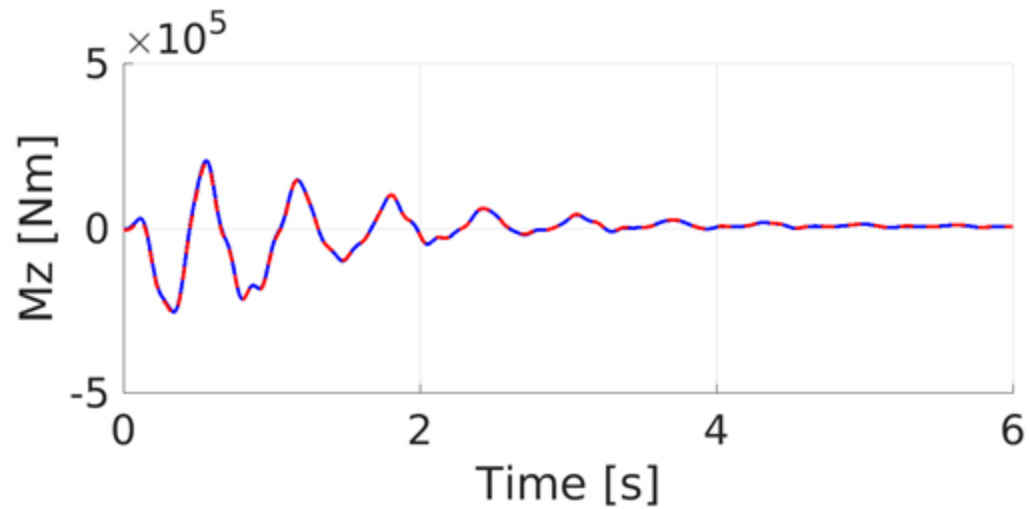
Define time step and duration

Extract loads from solution

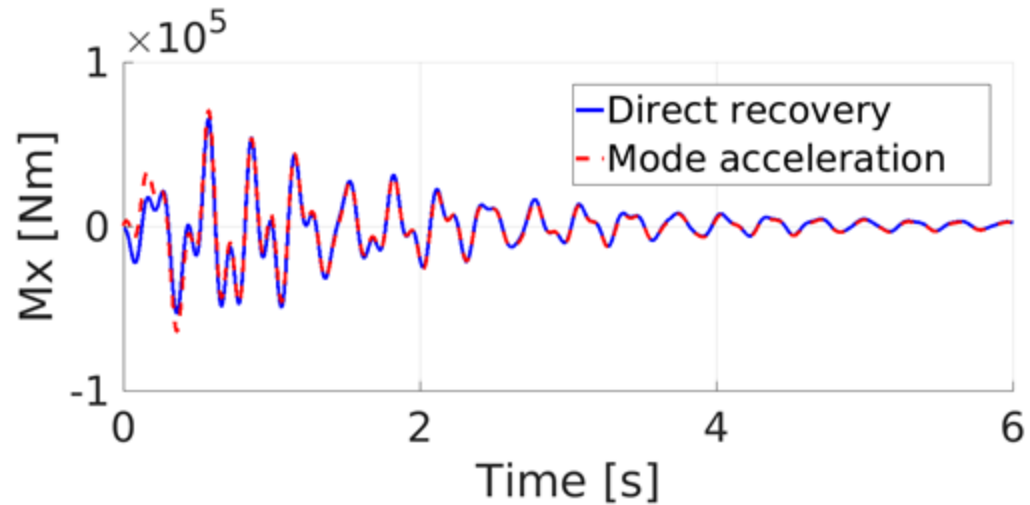


Elevator deflection response (4)

Wing root Bending moment



Wing root torsional moment



External load response (1)

This example shows how to simulate the response of an aircraft after an external load applied on two wing nodes in the z-direction

The following files are used in this portion of the tutorial:

- `inputMain_dload.dat` : Smartcad input file
- `exampleMain_dload.m` : Matlab script



External load response (2)

Smartcad input file

```
[...]  
SOL 146  
$  
PARAM      MODACC      0  
PARAM      VREF 170.000  
PARAM      RHOREF 1.22500  
PARAM      MACH 0.50000  
[...]  
$-----2-----3-----4-----5-----6-----7-----8-----9-----10  
LOAD= 1      2  
$-----2-----3-----4-----5-----6-----7-----  
$ Force input  
$-----2-----3-----4-----5-----6-----7-----  
$      ID      NODE      DOF      AMPLIT  TMAX  DELAY  
DLOAD  1      2002      3      1.0e+3  0.1  0.2  
      (1-cos(2*pi/0.1*t))*0.5  
$      ID      NODE      DOF      AMPLIT  TMAX  DELAY  
DLOAD  2      2020      3      1.0e+3  0.1  0.2  
      (1-cos(2*pi/0.1*t))*0.5
```

Enable load recovery with mode acceleration

Select the ID used in simulation among the IDs of the DLOAD cards. The effects of the two loads will be superimposed



External load response (3)

Matlab script (no variation w.r.t. gust response!)

```
global beam_model
global dyn_model

filename_sma = 'inputMain_dload.dat';

init_dyn_model(filename_sma)

solve_free_lin_dyn('dT', 5e-3, 'Tmax', 6);

positionWR_global = find(beam_model.Bar.ID==2002);
positionWR_results = find(beam_model.Param.IFORCE==positionWR_global);

wrbm_dirrec = squeeze(dyn_model.Res.IFORCE(6,1,positionWR_results,:));
wrbm_modac = squeeze(dyn_model.Res.MODACC.IFORCE(6,1,positionWR_results,:));
wrtm_dirrec = squeeze(dyn_model.Res.IFORCE(4,1,positionWR_results,:));
wrtm_modac = squeeze(dyn_model.Res.MODACC.IFORCE(4,1,positionWR_results,:));
```

Define time step and duration

Extract loads from solution



External load response (4)

```
>> dyn_model.Res
```

```
ans =
```

```
Extload_profile: [2x1201 double]
    Time: [1x1201 double]
    Qload: [20x1201 double]
    Qextf: [20x1201 double]
        Q: [20x1201 double]
        Qd: [20x1201 double]
        Qddot: [20x1201 double]
    Cy_mode: [1x1201 double]
    Cz_mode: [1x1201 double]
    Cl_mode: [1x1201 double]
    Cm_mode: [1x1201 double]
    Cn_mode: [1x1201 double]
        DISP: [512x6x1201 double]
    VELOCITY: [2x6x1201 double]
    ACCELERATION: [2x6x1201 double]
        IFORCE: [4-D double]
    HF_mode: [5x1201 double]
    MODACC: [1x1 struct]
```



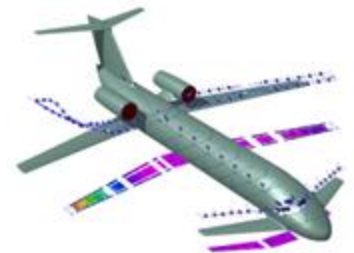
State-space model generation

It is possible to use NeoRESP to generate a linear state-space model of the aeroelastic system at a given flight condition.

The operation requires the definition of a complete solution for

- Modal analysis
- Unsteady aerodynamic

And thus can be performed as a post-processing of a dynamic response procedure

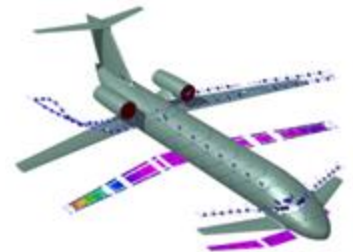


State-Space realization

The DLM provides the aerodynamic forces in the following format

$$f_a = q_\infty H_{am}(j\omega)q + q_\infty H_{ag}(j\omega)v_g + q_\infty H_{a\delta}(j\omega)\delta_c$$

- f_a Aerodynamic forces;
- q_∞ Dynamic pressure;
- q Modal coordinates;
- v_g Gust velocity;
- δ_c Control surface deflection;



State-Space realization

Each subsystem can be expressed in state-space form

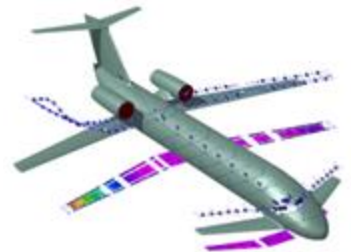
$$f_{am} = q_{\infty} H_{am}(j\omega) q$$

becomes

$$\begin{cases} \dot{x}_{am} = A_{am} x_{am} + B_{am}^0 q + B_{am}^1 \dot{q} + B_{am}^2 \ddot{q} \\ \frac{f_{am}}{q_{\infty}} = C_{am} x_{am} + D_{am}^0 q + D_{am}^1 \dot{q} + D_{am}^2 \ddot{q} \end{cases}$$

A similar formulation can be obtained for f_{ag} and $f_{a\delta}$

A quasi-steady approximation can also be used, where only D_{am}^0 , D_{am}^1 and D_{am}^2 are defined



State-Space realization

The transfer function is by first approximated as a right or left Matrix Fraction Description

$$H(s) = D(s)^{-1}N(s) \quad \text{LMFD}$$

or

$$H(s) = N(s)D(s)^{-1} \quad \text{RMFD}$$

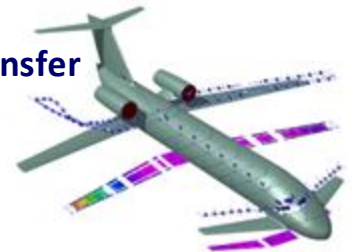
$D(s)$ is a matrix polynomial of order n

Number of states in the generated model:

- LMFD $\rightarrow n \times n_{forces}$ states;
- RMFD $\rightarrow n \times n_{inputs}$ states;

Reference:

Ripepi, M., and P. Mantegazza. "Improved Matrix Fraction Approximation of Aerodynamic Transfer Matrices." *AIAA journal* 51.5 (2013): 1156-1173.



Generation of the state-space aerodynamics

The aerodynamic system is generated using the function

```
ssAeroModel = getAeroModel(options)
```

The options can be defined either programmatically (as name/value pair) or through the use of a gui. The programmatic method will be demonstrated in the example matlab script. For allowing the definition of the parameters the function must be called as

```
ssAeroModel = getAeroModel([], 'useGUI', true)
```

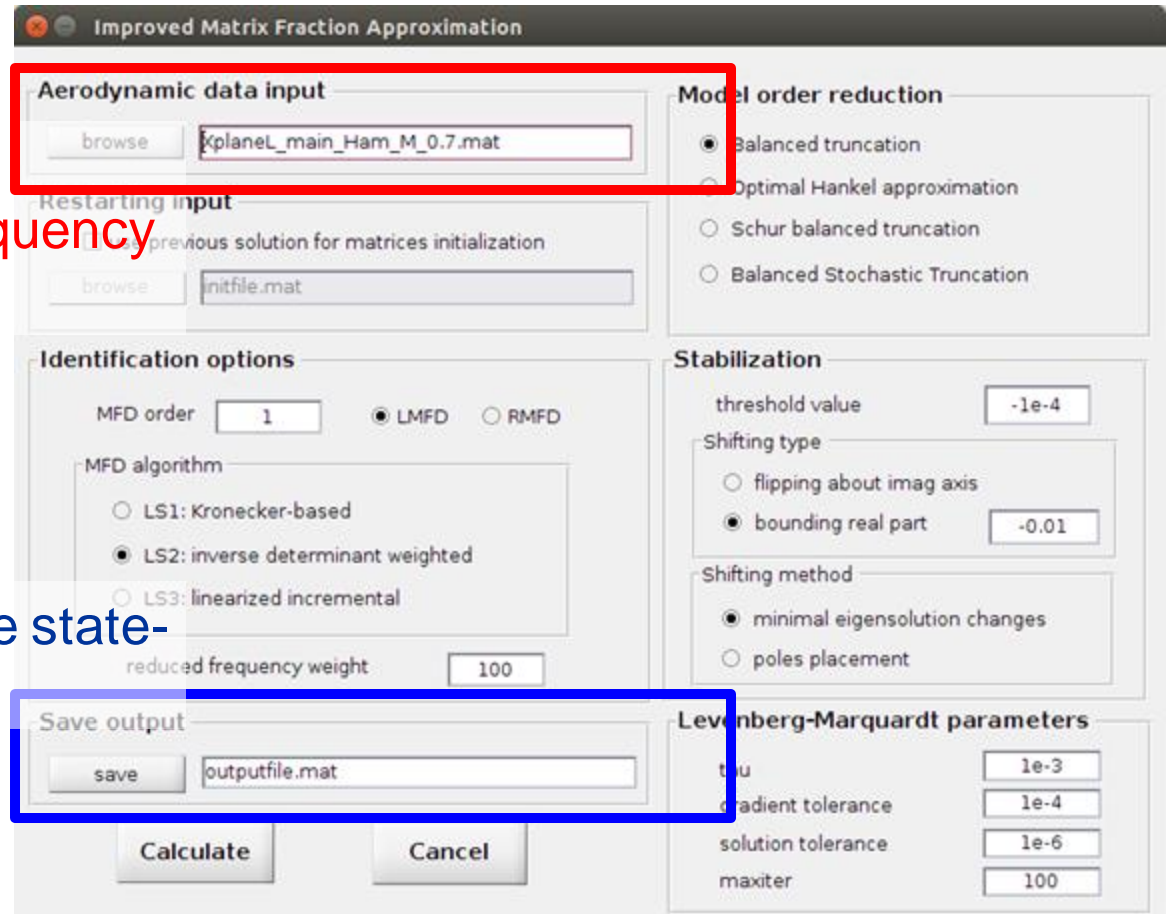
Not all the options available can be set using the GUI



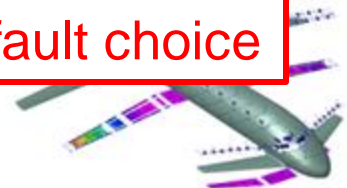
GUI – input and output files

INPUT: .mat file with the aerodynamic matrix in frequency domain

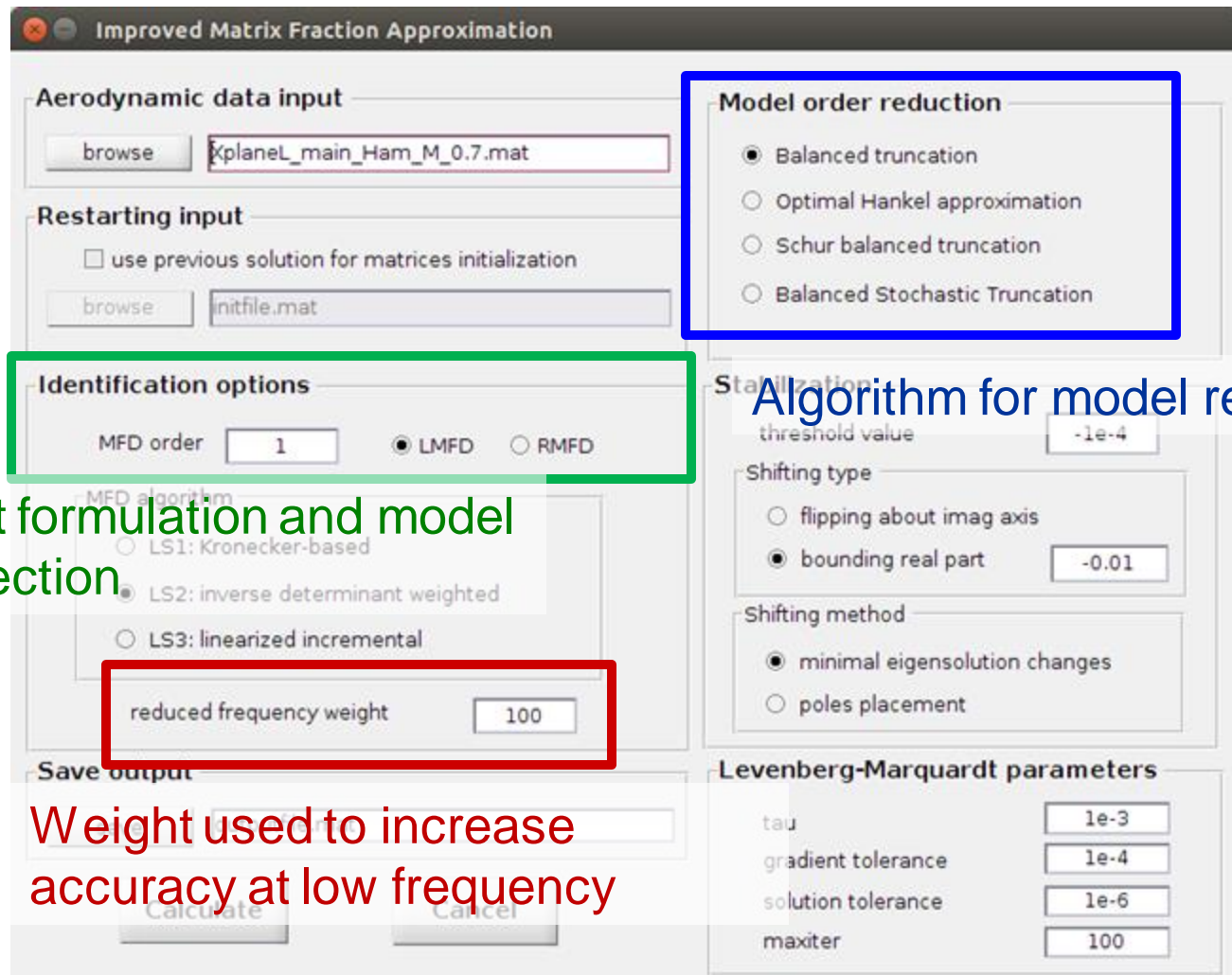
OUTPUT: .mat file with the state-space model



The function `getAeroModel` takes care of defining the correct file names, the user should not select a file different from the default choice

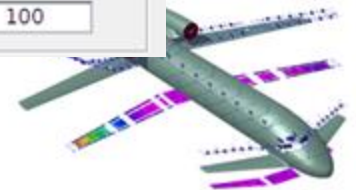


GUI – main parameters



Right/Left formulation and model order selection

Weight used to increase accuracy at low frequency



Model Reduction Phase

Increasing the order of the polynomial the accuracy of the state-space model increases, but can lead to a system with many states which have small effect in the input-output relationship. A model reduction procedure is applied to remove these states.

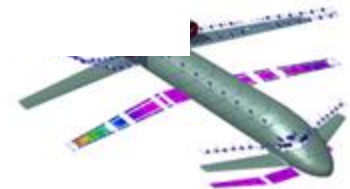
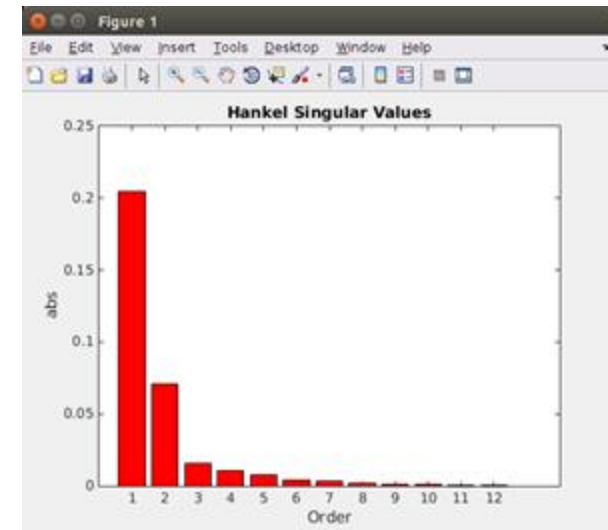
```
Check stability of state-space system: stable
```

```
(E,C) refitting before model order reduction:
```

```
-----  
error: 1.452168e-01
```

```
Model order reduction:
```

```
-----  
Please enter the desired order: (>=0) █
```



Options for SS model generation

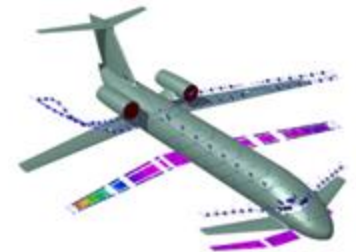
```
>> setAeroSSoptions();
```

Available options for the ss model generation:

```
    input : Input to aerodynamic system ('modal', 'gust', 'control')
    output : Output from aerodynamic system ('modal')
    selIn  : Select among input variables
    selOu  : Select among output variables
    mach   : Selection of Mach number
    kvect  : Selection of reduced frequencies (interpolation performed)
    method : Method for generation of the state space model ('mfd', 'qs')
    mfdOrder : MFD order (2)
    mfdAlg  : MFD algorithm (2)
    mfdSide : left or right MFD ('rmfd', 'lmfd') Used for reduced model
    mfdWeight : weight to enforce low frequency fitting (100) Used for reduced model
    mfdResOrder : order of residualization (2) automatically set to 2 with 'lmfd'
    mfdRollOff : roll off for discrete gust (2) (not used)
    LMtau   : tau: starting value for LM damping
    LMgradTol : tolerance on gradient
    LMsolTol : tolerance on solution variation
    LMmaxIter : Max num of iterations
    eigThres : threshold value for the eigenvalues real part
    eigMeth  : method for enforce stability ('eigshift', 'polesplace')
    eigType  : target poles ('bound', 'flip')
    igBound  : bound value
    algROM   : Model reduction algorithms: 'balance', 'hankel', 'schur', 'bst'
    rderROM  : Order for model reduction, if empty it will be requested during execution
    useGUI   : Use the gui for identification
    restartFile : Name of file used for restart
    kmin    : Minimum reduced frequency in QS approximation
    kmax    : Maximum reduced frequency in QS approximation
```

Method: 'mfd' is the matrix fraction method, 'qs' is the quasi-steady approximation

Enable the GUI (and discard all the mfd*, LM* eig* options)

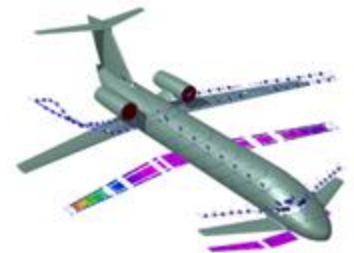


State-space model generation example

Smartcad input file (`inputMain_ss.dat`)

```
[...]  
$-----2-----3-----4-----5-----6-----7-----8-----9-----10  
GUST= 1  
SURFDEF= 1      2      3  
$-----2-----3-----4-----5-----6-----7-----8-----9-----10  
[...]
```

All the surface and gusts are selected in order to have them in the SS model



State-space model generation example

Matlab script (`inputMain_ss.dat`) – aerodynamic system definition

```
global beam_model
global dyn_model

SSopt_j = setAeroSSoptions([], 'method', 'mfd', ...
                            'mfdOrder', 2, ...
                            'selOu', {2:20, []}, ...
                            'selIn', {2:20}, ...
                            'kvect', kvectInterp, ...
                            'mfdweight', 100, ...
                            'mfdside', 'rmfd');

SSopt_g = setAeroSSoptions([], 'method', 'mfd', 'mfdOrder', 8);
SSopt_c = setAeroSSoptions([], 'method', 'mfd');

ssmodel_j = getAeroModel(SSopt_j, 'input', {'j'}, 'output', {'j','h'});
ssmodel_g = getAeroModel(SSopt_g, 'input', {'g'}, 'output', {'j','h'}, 'selOu', {2:20, []});
ssmodel_c = getAeroModel(SSopt_c, 'input', {'c'}, 'output', {'j','h'}, 'selOu', {2:20, []});

ssmodelArray = ssmodel_j;
ssmodelArray(2) = ssmodel_g;
ssmodelArray(3) = ssmodel_c;
% Assembly total aero model
ssmodel = assemblySSmodel(ssmodelArray, {'j', 'g', 'c'}, {'j','h'});
```

Initialize options

Compute the SS aerodynamic model. One for each type of input (modal, gust, control surface)

Merge all the aerodynamic SS models in a single system



State-space model generation example

Matlab script (`inputMain_ss.dat`) – flutter diagrams

```
% Check flutter diagram
[FLeigI, VvectI] = solve_linflutt_cont('Vmin', 20, 'method', 'continuation', 'axesUsed',
'inertial', 'selTracked', [7:20]);
[FLeigB, VvectB] = solve_linflutt_cont('Vmin', 20, 'method', 'pointwise', 'axesUsed', axesUsed);

l_a = dyn_model.dlm.aero.cref;
Vvect = {VvectB, VvectI};
FLeig = {FLeigB, FLeigI};
figHandleList = plotFlutterDiagram(Vvect, FLeig, l_a);
figHandle = figHandleList;
figHandle = flutterDiagramSSCorrected(dyn_model, Vvect{1}, ssmodel, figHandle, 'xg', l_a, ...
    'axesUsed', axesUsed, ...
    'seljUsed', seljUsed);
```

Computation with frequency domain aerodynamic

Computation with SS aerodynamic model

The comparison between the flutter diagrams obtained using time domain and frequency domain aerodynamic forces can be used to evaluate the accuracy of the identification.



State-space model generation example

Matlab script (`inputMain_ss.dat`) – generate SS model

```
% Assembly total aeroelastic model

[ssAEmodel_corr, aero, ssmodel, descrForm] = getAEmodelCorrected(dyn_model, ssmodel, ...
    'axesUsed', axesUsed, ...
    'seljUsed', seljUsed);

[...]

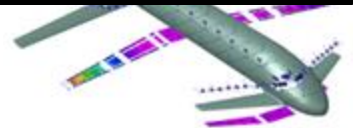
Dt = 1e-3; Tfin = 10;
Agust = 17.07; fgust = 2.5;
% Constant time step
T = 0:Dt:Tfin;
nT = length(T);

[...]

[TsC, YsC] = ssTimeSimulation(ssAEmodel_corr.A, ssAEmodel_corr.B(:,pos_input_corr), ...
    ssAEmodel_corr.C, ssAEmodel_corr.D(:,pos_input_corr),
    ag_tot, [], 0, Tfin, Dt, 'CN');
```

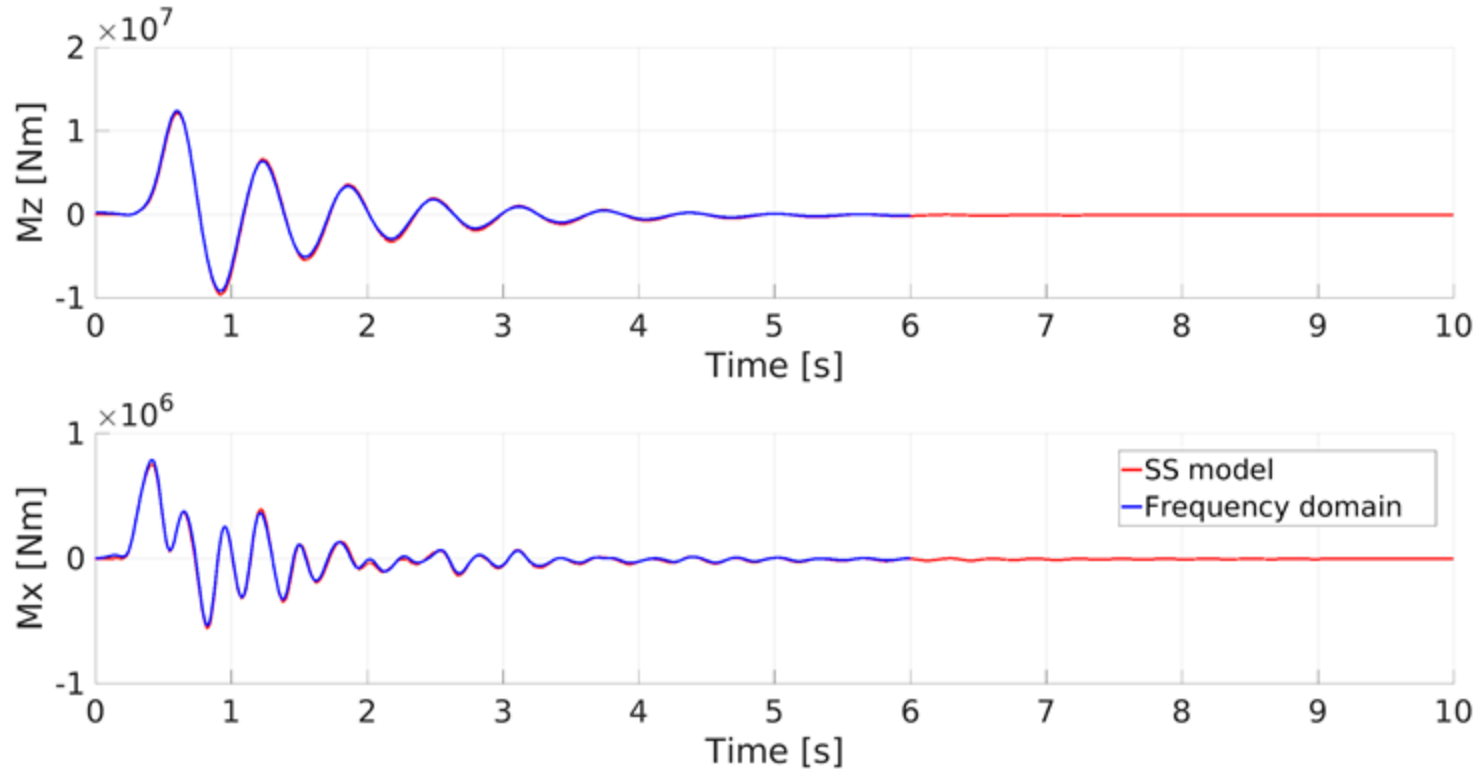
Name/value pair for defining
flight condition, modal base,
type of output ...

Time simulation



State-space model generation example

Comparison of results obtained from time-domain and frequency domain

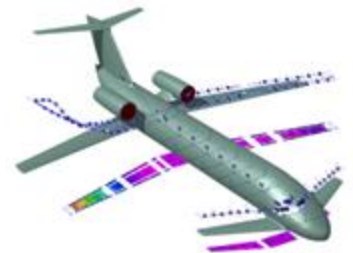


Aerodynamic mode correction

Among the options that can be set in the generation of the SS model there is also the possibility to introduce a set of aerodynamic coefficients to correct the steady portion of the aerodynamic forces.

```
[ssAEmodel_corr, aero, ssmodel, descrForm] = getAEmodelCorrected(dyn_model, ssmodel, ...  
    'aeroCoef', aeroCoef, ...  
    'axesUsed', axesUsed, ...  
    'seljUsed', seljUsed);
```

This capability is only described, but it is not included in the tutorial scripts.



Model output

The generated model is in a format compatible with the matlab SS class

```
ssAEmodel_corr =  
    A: [40x40 double]  
    B: [40x13 double]  
    C: [4085x40 double]  
    D: [4085x13 double]  
    inputGroup: [1x1 struct]  
    outputGroup: [1x1 struct]  
    inputName: {1x13 cell}  
    outputName: {1x4085 cell}  
    inputDelay: [13x1 double]
```

The model in the matlab SS class can be obtained using the function `convertToSS_neo`

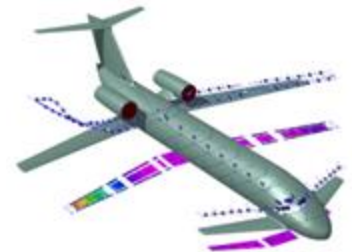
```
ssClassModel = convertToSS_neo(ssAEmodel_corr);
```

The system outputs are divided in groups

```
>> ssAEmodel_corr.outputGroup  
    accel: [1 2 3 4 5 6 7 8 9 10 11 12]  
    modalDisp: []  
    modalVel: []  
    displ: [1x3072 double]  
    vel: [1x12 double]  
    barforce: [1x984 double]  
    beamforce: []  
    aeroangles: []  
    modalForce: []  
    hingemom: [4081 4082 4083 4084 4085]
```

To each output a name is assigned

```
>> ssAEmodel_corr.outputName{ssAEmodel_corr.outputGroup.barforce(1)}  
ans =  
FORCE-BAR-1000-1-C1  
  
>> ssAEmodel_corr.outputName{ssAEmodel_corr.outputGroup.displ(1)}  
ans =  
DISP-1000-C1  
  
>> ssAEmodel_corr.outputName{ssAEmodel_corr.outputGroup.hingemom(1)}  
ans =  
HMOM-aileronr
```



Definition of aerodynamic coefficients

```

aeroCoef.system = 'stability';
aeroCoef.aeroType = 'aero';
aeroCoef.inputType = 'angles';
aeroCoef.refPoint = [13.463, 0, 1.8275];
aeroCoef.cref = 2.5642;
aeroCoef.bref = 29.654;
aeroCoef.Sref = 73.276;

aeroCoef.Mach = [0.3, 0.52];
    
```

- Reference system used for the definition of coefficients
- Reference point for the definition of aerodynamic moments
- Reference dimensions for nondimensionalization
- Mach number used for the definition of the coefficients

```

aeroCoef.F0(:, :, 2) = [
    0.0379;
    0;
    0.337;
    0;
    0.06;
    0];
    
```

Forces at reference condition

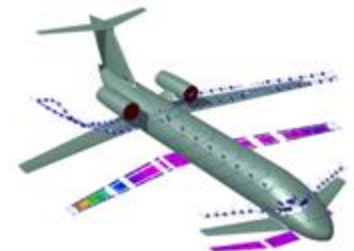
```

aeroCoef.C0 = zeros(6,6,2);
aeroCoef.C0(:, 2:6, 1) = [
    0, 0.0382, 0, 0.0861, 0;
    1.17, 0, -0.06, 0, 0.666;
    0, 6.486, 0, 14.6, 0;
    -0.176, 0, -0.594, 0, 0.123;
    0, -1.534, 0, -70.48, 0;
    0.106, 0, -0.052, 0, -0.231];
    
```

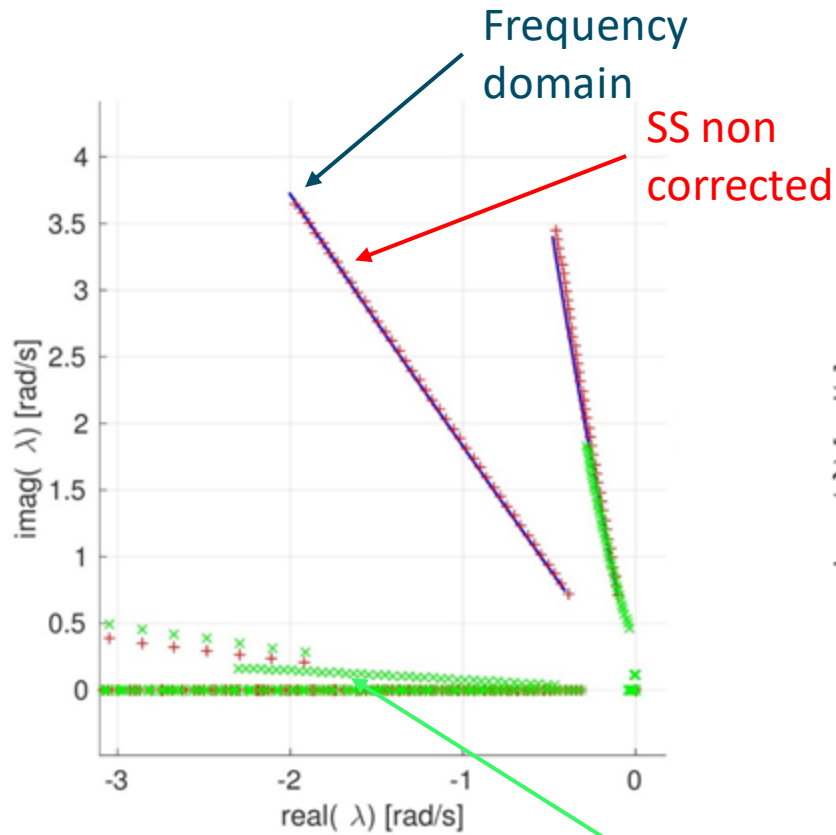
Aero coefficients for each Mach number

```

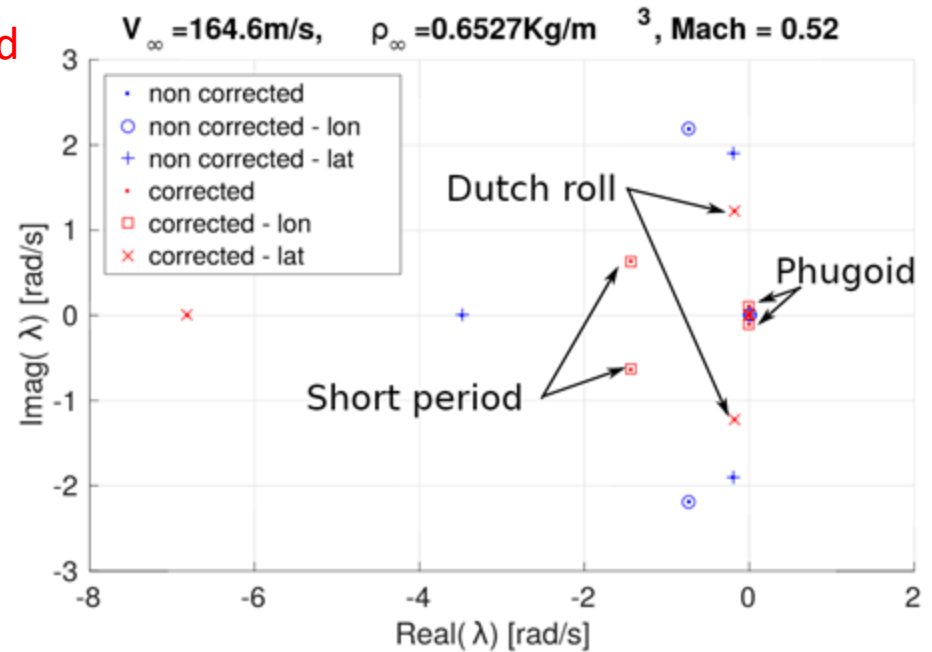
aeroCoef.C0(:, 2:6, 2) = [
    0, 0.0471, 0, 0.0959, 0;
    1.20, 0, -0.06, 0, 0.666;
    0, 7.173, 0, 14.6, 0;
    -0.180, 0, -0.625, 0, 0.113;
    0, -0.15, 0, -68.53, 0;
    0.115, 0, -0.042, 0, -0.244];
    
```



Example of results (on a different model)



SS Corrected



Thanks for your attention

